Brief communication: Pancake ice floe size distribution during the winter expansion of the Antarctic marginal ice zone

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Abstract.

The size distribution of pancake ice floes is calculated from images acquired during a voyage to the Antarctic marginal ice zone in the winter expansion season. Results show that 50% of the sea ice area is made up by floes with diameters 2.3–4 m. The floe size distribution shows two distinct slopes on either side of the 2.3–4 m range, neither of which conforms to a power law. Following a relevant recent study, it is conjectured that growth of pancakes from frazil forms the distribution of small floes ($D < 2.3$ m), and welding of pancakes forms the distribution of large floes ($D > 4$ m).

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1 Introduction

Prognostic floe size distributions are being integrated into the next generation of large-scale sea ice models (Horvat and Tziperman, 2015; Zhang et al., 2015, 2016; Bennetts et al., 2017; Roach et al., 2018a). Early results show that the floe size distribution affects ice concentration and volume close to the ice edge, in the marginal ice zone, where ocean waves regulate floe sizes and floes are generally the smallest, meaning they are prone to melting in warmer seasons (Steele, 1992). However, at present the only field data available to validate and improve the models are empirical distributions derived for pack ice spanning several orders of magnitude (from few meters to tens of kilometres; e.g. Toyota et al., 2016) and none resolve floes below the meter scale.
Break up of pack ice often resembles a fractal behaviour similar to many brittle materials (Gherardi and Lagomarsino, 2015). It has been argued that exceedance probability of the characteristic floe size, \( D \), expressed as number of floes, follows a power law \( N(D) \propto D^{-\alpha} \), where the scaling exponent is \( \alpha = 2 \) if a fractal behaviour is assumed (Rothrock and Thorndike, 1984).

Most of the previous observations of the floe size distribution in the marginal ice zone (noting that no observations are in pancake ice conditions) conform to a truncated power law (Stern et al., 2018), with the \( \alpha \) value varying among studies depending on season, distance from the ice edge and range of measured diameters. Some support observations of floe size distributions have been interpreted using a split power law (e.g. Toyota et al., 2016), with a mild slope for smaller floes and a steeper one for larger floes. In most cases, the sharp change in slope is an artefact due to finite size effects (Stern et al., 2018), although in few instances the split power law behaviour might be consistent with the data (Stern et al., 2018). The truncated power law cannot explain two different slopes in the probability density function \( n(D) \), suggesting that different mechanisms might in fact govern the distributions for small and large floes (Steer et al., 2008; Toyota et al., 2011).

The validity of the power law scaling has been verified for most cases but its universality has not been demonstrated yet (Horvat and Tziperman, 2017) and its adoption is mostly justified by the wide range of floe diameters. Scaling parameters are typically estimated on the log-log plane with a least square fit, which leads to biased estimates of \( \alpha \), and, as noted by Stern et al. (2018), without rigorous goodness-of-fit tests. In comparison, Herman et al. (2018) examined the size distribution of floes under the action of waves in controlled laboratory experiments, by analysing the probability density function \( n(D) \), which revealed a fractal response due to an arbitrary strain (a power law) superimposed to a Gaussian break up process induced by the waves. The interplay of these mechanisms is hidden in the floe number exceedance probability.

Existing observations do not provide quantitative descriptions of the floe size distribution for pancake ice floes, which form from frazil ice under the continuous action of waves and thermodynamic freezing processes (Shen et al., 2004; Roach et al., 2018b). This is important, for example, during the Antarctic winter sea ice expansion, when hundreds of kilometres of ice cover around the Antarctic continent is composed of pancake floes of roughly circular shape and characteristic diameters 0.3–3 m (Worby et al., 2008). Pancake floes represent most of the Antarctic sea ice annual mass budget (Wadhams et al., 2018). Moreover, in the Arctic, pancakes are becoming more frequent than in the past due to the increased wave intensity associated with the ice retreat (Wadhams et al., 2018; Roach et al., 2018b).

Shen and Ackley (1991) reported pancake floe sizes from aerial observations collected during the Winter Weddell Sea Project (July 1986), showing that pancake sizes increase with distance from the ice edge, from 0.1 m in the first 50 km up to \( \approx 1 \) m within 150 km from the edge (but without investigating the floe size distribution). They attributed this to the dissipation of wave energy with distance into the ice-covered ocean, and proposed a relationship between wave characteristics, mechanical ice properties and pancake size (Shen et al., 2004). More recently, Roach et al. (2018b) used camera images acquired from SWIFT buoys deployed in the Beaufort Sea (Sea State cruise, October–November 2015) to quantify the lateral growth of pancakes and their welding. A correlation between wave properties and the size of relatively small pancakes (up to 0.35 m) was confirmed.
To our knowledge, the pancake floe size distribution has yet to be characterised, noting that although Parmiggiani et al. (2017) developed an algorithm for pancake floes detection, they did not provide quantitative indication on the shape and size of the floes. Here, a new set of images from the Antarctic marginal ice zone are used to measure the shape of individual pancakes and to infer their size distribution.

2 Sea ice image acquisition

Environmental condition during on the 4th of July 2017 (local time UTC +2). Peak wave period (a) and significant wave height (b) are sourced from ECMWF ERA-Interim reanalysis. The magenta area denotes ice and grey dots show the ship track. In (c), which is the subdomain indicated by a white frame in (a) and (b), ice concentration is sourced from AMSR2 satellite with a 3.125 km resolution (Beitsch et al., 2014). The black dots denotes the position during which cameras were operational and measurements undertaken. The green cross the location of deployment of a wave buoy. In (d), pancake floe concentration reconstructed from the camera images is shown as black dots, and total ice concentration obtained from AMSR2 satellite at the location closest to the measurements is shown as magenta squares.

At approximately 07:00 UTC on the 4th of July 2017, the icebreaker S.A. Agulhas II entered the marginal ice zone between 61° and 63° South and approximately 30° East during an intense storm (see Fig. 1a,b for the ship track and a snapshot of peak wave period and significant wave height as sourced from ECMWF ERA-Interim reanalysis, Dee et al. 2011). A buoy was deployed in the marginal ice zone ≈ 100 km from the ice edge (green mark in Fig. 1c). At the time of deployment, the significant wave height was 5.5 m, with maximum individual wave height of 12.3 m. The dominant wave period was 15 s.

A system of two GigE monochrome industrial CMOS cameras with a 2/3 inch sensor was installed on the monkey bridge of the icebreaker to monitor the ocean surface. The cameras were equipped with 5 mm C mount lenses (maximum aperture f/1.8) to provide a field of view of approximately 90°. The cameras were installed at an elevation of ≈ 34 m from the waterline and with their axes inclined at 20° with respect to the horizon. The system was operated by a laptop computer. Images were recorded with resolution of 2448×2048 pixels and a sampling rate of 2 Hz during daylight on the 4th of July (from 07:00 to 13:30 UTC).

Sample acquired image (a), rectified and calibrated image (b) and detected pancakes (c).

An automatic algorithm was developed using the MatLab Image Processing Toolbox (Kong and Rosenfeld, 1996) to extract sea ice metrics from the recorded images (see Fig. 2a for an example). To ensure statistical independence of the data set (i.e. to avoid sampling the same floe twice), only one camera and one image every 10 s was selected for processing (this interval guarantees no overlap between consecutive images). Images were rectified to correct for camera distortion and to project them on a common horizontal plane. A pixel to meter conversion was applied by imposing camera-dependent calibration coefficients. The resulting field of view is 28 m×28 m and resolution 29 px/m (see Fig. 2b). The image was processed to eliminate the vessel from the field of view, adjust the image contrast, and convert the grey scales into a binary map based on a user selected threshold. The mapping isolates the solid ice shapes from background water or frazil ice. The binary images, however, are noisy and require refining based on morphological image processing to improve the shape of the pancakes fidelity.
and the associated drift of the ice edge (detection of pancake ice only). Moreover, satellite data are an average over two daily swaths. Due to the intense storm activity the AMSR2 concentration includes the interstitial frazil ice, which is intentionally excluded from the image processing (i.e. the subdomain indicated by a white frame in (a) and (b), ice concentration is sourced from the AMSR2 satellite with a 3.125 km resolution (Beitsch et al., 2014). The black dots denote the position during which cameras were operational and measurements undertaken. The green cross denotes location of deployment of a wave buoy. In (d), pancake floe concentration reconstructed from the camera images is shown as black dots, and total ice concentration obtained from AMSR2 satellite at the location closest to the measurements is shown as magenta squares.

Identification of individual pancakes allows estimation of the individual floe areas $S$. An overall ice concentration ($i_c$, Fig. 1d) can be computed as the ratio of the area covered by pancake floes to the total surface in the field of view. A representative concentration was estimated every 60 consecutive images (i.e. 10 min time window), which is equivalent to a sampled area of 0.047 km². Pancake concentration was consistently $\approx 60\%$ with no significant variations throughout the day (Fig. 1d). The observed pancake concentration diverged from satellite observations (AMSR2) of sea ice concentration (see Fig. 1d), as the AMSR2 concentration includes the interstitial frazil ice, which is intentionally excluded from the image processing (i.e. detection of pancake ice only). Moreover, satellite data are an average over two daily swaths. Due to the intense storm activity and the associated drift of the ice edge ($\approx 100$ km Eastward in a day) at that time, this average may not be fully representative of
the instantaneous conditions, resulting in underestimation of the encountered ice concentration. In this regard, bridge observations following the Antarctic Sea Ice Processes and Climate protocol (ASPeCt, Worby et al., 2008), indicated a 90–100% concentration of total ice, where pancake ice was the primary ice type with concentration of 50–60% for most of the cruise (de Jong et al., 2018), in agreement with the image processing.

3 Pancake ice shape and floe size distribution

In (a), scatter plot of the major and minor axis of the pancake floe with the linear fit (solid orange line), the inset shows the probability density function of $D_1/D_2$. In (d), scatter plot of the circularity of the floes against the equivalent diameter and the average value (solid orange line). In (b), ice area distribution as a function of the floe diameter expressed as exceedance probability. In (e), ice area distribution as a function of the floe diameter expressed as probability density function. In (c), floe number exceedance probability $N(D)$ as a function of the floe diameter with two power law (solid orange lines) fitted for small ($D < 2.3 \text{ m}$) and large floes ($D > 4 \text{ m}$) respectively. In (f), floe number probability density function $n(D)$ as a function of the floe diameter with two power law (solid orange lines) fitted for small ($D < 2.3 \text{ m}$) and large floes ($D > 4 \text{ m}$) respectively.

Approximating the floe shape as an ellipse, major ($D_1$) and a minor ($D_2$) axes are extracted. It is common practice, however, to define one representative dimension as a characteristic diameter $D = \sqrt{4S/\pi}$, by assuming that the pancake is a disk (Toyota et al., 2016), noting that other metrics are also widely used, e.g. the mean caliper diameter (Rothrock and Thorndike, 1984). Only floes entirely within the field of view are considered for these operations. Detection of small floes with $D < 0.25 \text{ m}$ is prone to error due to the limited number of pixels of which these floes are comprised and, thus, excluded from the analysis (Toyota et al., 2011). Moreover, a small fraction of large floes (< 10% of floes larger than 5 m) were artificially welded by the image processing. These floes were also excluded. In total, $4 \times 10^5$ individual floes were considered over an equivalent sampled area of $\approx 1.55 \text{ km}^2$, and spanning almost 100 km of non-contiguous marginal ice zone.

Fig. 3a presents a scatter plot of the aspect ratio ($D_1 : D_2$). On average $D_1$ is $\approx 60\%$ greater than $D_2$ (slope of a linear fit). This aspect ratio is similar to one observed for broken ice floes (Toyota et al., 2011). The inset shows the full probability distribution of the ratio $D_1/D_2$ and indicates that floes elongated such that $D_1/D_2 > 3$ are infrequent. Fig. 3d shows the...
In transition from mild to steep slopes around the dominant diameter of 3.1 m. The probability density function of the equivalent to floe regimes are defined as \( D_1 \) and \( D_2 \). In (b), ice area distribution as a function of the floe diameter expressed as exceedance probability. In (c), floe number exceedance probability \( N(D) \) as a function of the floe diameter with two power laws (solid orange lines) fitted for small \( D < 2.3 \) m and large floes \( D > 4 \) m respectively. In (d), scatter plot of the circularity of the floes against the equivalent diameter and the average value (solid orange line). In (e), ice area distribution as a function of the floe diameter expressed as probability density function. In (f), floe number probability density function \( n(D) \) as a function of the floe diameter with two power laws (solid orange lines) fitted for small \( D < 2.3 \) m and large floes \( D > 4 \) m respectively.

Circularity \( C = 4\pi S/P^2 \), where \( P \) is the floe perimeter (for a circle \( C = 1 \)), which characterises the shape of the floes, noting that other metrics can be used to define the roundness of the floes (Hwang et al., 2017). For floes up to \( D \approx 6 \) m, the average circularity, denoted by the continuous line, is \( C \geq 0.75 \). Similar values have been reported for much larger broken floes (Lu et al., 2008).

Fig. 3b and 3e display the floe size area distribution as exceedance probability and probability density function respectively. Fig. 3e shows that, in terms of the equivalent diameter \( D \), 50% of the pancake area is comprised of floes with diameters in the range 2.3–4 m. The mode of the area distribution is 3.1 m (median and mean are \( \approx 3.1 \) m and \( \approx 3.2 \) m respectively), compared to \( D_1 = 4 \) m and \( D_2 = 2.6 \) m using the major and the minor axes.

Fig. 3c shows the exceedance probability \( N(D) \), which exhibits two distinct slopes in the log-log plot, with a smooth transition from mild to steep slopes around the dominant diameter of 3.1 m. The probability density function of the equivalent diameter \( n(D) \), shown in Fig. 3f, displays a pronounced hump in the transition between these regimes, revealing a third regime \((2.3 m < D < 4 m)\) around the modal pancake diameter, which is hidden in the exceedance probability, where the small- and large-floe regimes are defined as \( D < 2.3 \) m and \( D > 4 \) m (somewhat arbitrarily).
Small floes \((D < 2.3 \, \text{m})\) constitute the vast majority of the total detected floes (>80%). In this regime, the mild slope of \(N(D)\) may result from a continuous process of floes accretion (from frazil to larger pancakes) regulated predominantly by thermodynamic freezing processes (Roach et al., 2018b). Floes larger than 4 m are detected far less frequently (<5% of the total floes), and the steeper slope indicates that their size is most likely governed by different underlying physical mechanisms. Visual examination of the acquired images shows that the majority of the large floes are composed of two or more welded pancakes suggesting that the welding process, promoted by the high concentration of pancakes and the presence of interstitial frazil ice (Roach et al., 2018b), could be the dominant underlying mechanism for the shape of the probability distribution of large floes. Finite size effects are ruled out because the change in slope occurs for \(D \approx 4\) m which is considerably smaller than the image footprint.

Assuming, as standard, a power law \(N(D) \propto D^{-\alpha}\) as a benchmark and using the maximum likelihood method following Stern et al. (2018), we determine \(\alpha = \alpha_S = 1.1\) for small floes \((D < 2.3 \, \text{m})\) and \(\alpha = \alpha_L = 9.4\) for large floes \((D > 4 \, \text{m})\). (Note that the maximum recorded diameter was \(D = 10.8\) m, and, therefore, the estimation of the scaling exponent is rigorously not applicable not particularly meaningful or robust in either of the two regimes, as less than a decade of length scales are available.)

The power-law fits are approximations only, and an objective Kolmogorov–Smirnov goodness-of-fit test (Clauset et al., 2009) reveals that the empirical pancake size distribution does not scale accordingly to a power law in either the small- or large-floe regime, noting the power law hypothesis is more likely to be rejected when tested over limited diameter ranges (i.e. less than a decade). A close inspection of the empirical distribution shows that \(N(D)\) possesses a slightly concave-down curvature across all the diameter ranges (in a log-log plane), which is commonly associated with a truncated power law (Stern et al., 2018). The corresponding \(n(D)\) displays an S-shape in the small-floe regime (it shifts from a concave-down to a concave-up curvature at \(D \approx 1 \, \text{m}\)) in contrast to the hypothesis of a power law behaviour. Deviations from the power law scaling are prominent towards the extremes of the intervals \((D \to 0.25 \, \text{m} \text{ and } D \to 2.3 \, \text{m} \text{ for the small-floe regime; } D \to 4 \, \text{m} \text{ and } D \to 10 \, \text{m} \text{ for the large-floe regime})\) but become conspicuous only by examining the empirical distribution over limited diameter ranges and probability intervals (i.e. zooming in on Figs. 3c–f). We also note that the increasing \(a(D)\) in the small-floe regime (see Figs. 3e) is inconsistent with a power law with for \(\alpha_S \geq 1\) and, thus, the area as the area and number distributions are proportional to each other, i.e. \(a(D) \propto D^2 n(D)\). Values of \(\alpha_S \geq 1\) may be because the exponent has been estimated over a range of less of decade of diameters making its estimation non-robust. The discrepancy between area and number distribution confirms that the underlying number distribution is not a power law, although we note that \(\alpha_S \in (0.9, 1)\) provides a qualitatively good fit for the number distribution and is consistent with growing area distribution.

Goodness-of-fit tests also rule out floe size distributions such as the truncated power law (Stern et al., 2018), generalized Pareto (Herman, 2010), and linear combination of Gaussian distribution and power law (Herman et al., 2018). It appears that an accurate approximation of the floe size distribution (in the goodness-of-fit sense) can only be achieved by dropping any a priori assumptions on the functional shape, e.g. by using a nonparametric kernel density estimation (Botev et al., 2010). However, this does not provide any insight on the underlying physical processes responsible for the shape of the empirical distribution.
4 Conclusions

Observations of pancake ice floe sizes during the winter expansion of the Antarctic marginal ice zone were analysed. An automatic floe detection algorithm was used to extract metrics (diameter and area) of the pancake floes, for which the equivalent diameter \( D = \sqrt{4S/\pi} \) ranged between 0.25–10 m. This allowed a quantitative representation of the pancake size distribution to be discussed.

The floe size distribution displays three distinct regimes, which are visible in the probability density function that, compared to the commonly reported exceedance probability, is more informative. One regime is \( D = 2.3–4 \) m, centred around the dominant pancake diameter of 3.1 m, which covers half of the total pancake area, and appears as a hump in the probability density function. Two different behaviours are observed for smaller and larger pancakes on a log-log plane. The small-floe regime \( (D < 2.3 \) m), in which it is conjectured that pancakes are experiencing thermodynamic growth, is characterised by a mild negative slope (in terms of the floe number exceedance and probability density function), while the large-floe regime, in which floes are typically formed by welding (detected from visual analysis), is characterised by a much steeper slope noting that neither of the two regimes conform to a power law scaling.

These results reflect observations collected under storm conditions and, thus, lack generality. Simultaneous measurements of waves, floe size and heat fluxes under a number of different conditions are needed to verify the conjecture that different physical mechanisms (e.g. thermodynamic growth and welding) are responsible for the peculiar shape of the pancake ice floe size distribution.

Code and data availability. The detection algorithm and the acquired images are available upon request to the corresponding author.

Competing interests. The authors declare that they have no conflict of interest.

Appendix A: Pancake detection algorithm

The algorithm for the pancake detection is developed using the MatLab Image Processing Toolbox and built-in functions.

1. Rectification: projects the distorted camera image on an horizontal plane based on the camera internal parameters and the angle of view;

2. Contrast adjustment: contrast in the greyscale image is enhanced based on a CLAHE algorithm (the limit for clipping and shape of the distribution are user selected) to better isolate the pancakes from the frazil ice;

3. Masking: removes the ship from the field of view;
4. **Binary conversion**: the greyscale image is converted into a binary image where 1 corresponds to white (i.e., ice) and 0 to water or frazil (the threshold for conversion is user selected);

5. **Cleaning**: this morphological operation removes isolated white pixels (i.e., 1s completely surrounded by 0s);

6. **Erosion**: this morphological operation helps to separate the blobs corresponding to the pancakes (the erosion value is user selected);

7. **Filling**: this morphological operation substitute 0s with 1s in area completely enclosed by white pixels;

8. **Dilatation**: this morphological operation counterbalance the ice pixels lost by the erosion without merging two separate blobs;

9. **Clear border**: removes blobs intersecting the border of the field of view;

10. **Labelling and properties extraction**: geometrical properties of each individual floe are extracted.

All thresholds are user selected and the parameters have been subjected to testing to find the combination of operations that provided the best reconstruction as evaluated by the user visual inspection.

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References


Comments to the Author:

In my view, the author’s have sufficiently addressed all the reviewer comments. Although reviewer #2 indicated major changes, it appears to me that most of the comments required minor changes to the text and have been adequately addressed.

Response to the Editor:

We thank the Editor for the positive feedback.

There is one comment, however, that I do not feel the author’s adequately explained:

Page 5, Figure 3. It looks to me like Figure 3b (the area distribution, a(D)) is not compatible with Figure 3d (the PDF, n(D)). In 3b, the area distribution increases as D increases, from D=0.2 to D=3. In that range, alpha_S = 1.1 so alpha_S + 1 = 2.1 so the PDF n(D) scales like D^-2.1. The area of a floe scales like D^2. So the area distribution a(D) should scale like D^(-2.1 + 2) = D^-0.1. That means the area distribution should DECREASE as D increases from D=0.2 to D=3. But Figure 3b shows a(D) increasing as D increases over that range. Is there something wrong with the plots, or with my analysis?

The authors’ response is that by changing the range over which alpha_S is determined, one could get different alpha_S because of the concavity of the area distribution. This is true (for example over D=1.5-3, one obviously), but does not explain why the a(D) increases monotonically from D=0.3-2.3 and the fit of alpha_S over that same interval results in alpha_S > 1. Based on the reviewer’s analysis, it alpha_S should be less than 1 over this precise interval. I believe this may be an issue with how robust the fit in Figure 3f is. From D=1.5-2, n(D) is flat, so a fit over this range would have alpha+1 ~1, and this is consistent with an increasing a(D) based on the reviewer’s analysis. But for D=0.3-1.5, alpha +1 looks to be slightly less steep than the red line fit in 3f, so alpha could be < 1 over this range as well, so that would also be consistent with a(D) increasing, although less steeply. That’s all fine. But since the red line fit is to 0.3-2.3, and the blue line appears less steep than this over both the 0.3-1.5 and 1.5-2.3 ranges, why is the red line, which is fit over the full range 0.3-2.3 steeper than what you would intuitively expect for a fit over either of these ranges? Is it due to the fitting technique? If so, then it would seem that this fit is not particularly robust. The authors’ response does not really answer why a(D) still increases over the full range of 0.3-2.3 yet the fit has alpha_S > 1.

Now what the exact value of alpha_S is is not so important for the main points of the paper, but this does suggest to me that there is a possible issue with the fit. This needs to be explained. The statement added to the text is too short, and doesn’t really explain why the increase in a(D) is inconsistent with alpha_S>1 for the reader.

Response to the Editor:

We use the power law fit, but the goodness of fit test reveals that the underlying distribution is not a power law.
In general $a(D) \sim D^2 n(D)$, but we can only write $a(D) \sim D^{-(\alpha+1)}$ if the number distribution is a power law, and, as pointed out by the reviewer and the editor, we obtain an increasing $a(D)$ only for $\alpha < 1$. However, the area distribution obtained assuming a power law provides inconsistent results because the underlying distribution is, in fact, not a power law. For example, we run few tests and the $n(D)$ is qualitatively comparable to an exponential in the small floe regime, which is consistent with an increasing area. If we assume $n(D) \sim \exp(-D)$ we get $a(D)$ increasing up to $D=2$, as $a(D) \sim D^2 \exp(-D)$ has derivative $(2-D) \cdot D \cdot \exp(-D)$, which is positive for $D<2$.

Moreover, having assumed a power law and applied a maximum likelihood method over a limited range of diameters (i.e. less than a decade), we doubt the robustness of the computed exponent, which might drop below 1 (in the revised manuscript we write that the less than a decade interval “is not particularly meaningful or robust”). By applying a less rigorous least square fitting, we find $\alpha \sim 0.9$, which is consistent with growing area distribution. Indeed, the qualitative fit does not vary dramatically for $\alpha$ values between 0.9 and 1.1 (see below).

**Minor edits/clarifications:**

*Line 2 change to “made up of floes”*

*Changed*

*Abstract – Based on the comments and your conclusions, I wonder if it is worth stating in the abstract that the FSD does not exhibit power law behavior?*

*Added*

*Page 2, Line 5 – are you sure that “most” of the observations conform to a truncated power law? I believe Stern et al (2018) only states that several studies show this, , or if only some conform to a truncated power law. Also, my understanding is that the “split power law” could be an artifact of this truncation (or finite size effects) – see figure 3 of Stern et al (2018). Your text as written could be read to imply that previous observations show either a*
truncated power law or split power law. But I believe many of the prior studies only suggest a single power law. Please clarify this statement.

As stated by Stern (2018), while the truncated power law fits most of the previous datasets, Stern (2018) does not exclude that in certain cases the split power law might consistent with the data (i.e. there is physical basis for the split power law). In particular, the truncated power law cannot describe the data of Steer (2008) in which the probability density function is shown, as discussed in Stern (2018) in 4.1 at the end of the first paragraph. We clarified these issues.

Page 2, Line 11-12 – despite your response to the reviewer, you still state that the power law scaling has not been demonstrated, and you still make the claim that the power-law scaling is justified by the wide range of diameters. Please modify the former to state that the power law has been demonstrated for only some cases, and the latter to state something more reasonable – isn’t it justified simply because it appears to follow a power-law, even if this is not rigorously verified?

We use “demonstrate” when it is mathematically proven. We agree that Stern has shown the truncated power law fits most of the previous observations, but this doesn’t constitute a proof. We write that the power law has been verified for most cases, but its universality has not been demonstrated yet.

Figure 1, caption – “Environmental conditions”

Figure 1, caption – “sourced from the AMSR2”

Figure 1, caption – “The black dots denote”

Page 4, line 17 – “image processing”

Page 4, line 19 – perhaps to better address the reviewer’s comment, this could be changed to “image processing to improve the fidelity of the shape of identified pancake floes”

Page 4, line 19 – “light and ice conditions”

Figure 3 caption – “floe diameter with two power laws”, “(D > 4m), respectively”. Also I think it would be better if the panels were described in order (i.e. a, b, c, d, e, and f).

Page 5, line 7 – be better to state that this could result in an over- or underestimation of the in situ ice concentration. There is no reason to expect this average would always cause an underestimation.

Page 6, line 28 – “transition between these regimes”

All changed.

Page 7, line 12-13 – are you sure you can say estimation of the scaling exponent it is not rigorously applicable because of the less than a decade of length scales? I am not certain, but I would guess that for a large amount of well-behaved observations, one could achieve a
rigorous fit (at least over that less-than-decade range). My point is “rigorously” might not be a precise word here. Perhaps better to say “not particularly meaningful”? Leave alone if it is correct.

Changed. We also added that it is probably not robust.

References – please ensure your references are consistent with The Cryosphere style. For instance, you have full journal titles, whereas journal style is to abbreviate.

Changed. We used bibtex in the Cryosphere style.

Page 9 line 7 – should annals be capitalized here?

Page 9, line 17 – Reports should be capitalized.

Page 9, line 20 – Herman et al. is now in The Cryosphere (https://www.the-cryosphere.net/12/685/2018/), so this reference should be updated.

Supplementary material – this supplement is quite short, so could this be better included as an appendix?

All changed.