We thank both referees for their thoughtful and thorough reviews of our paper. We appreciate you taking the time to complete these reviews and welcome your helpful comments. We have revised the manuscript to address your review comments (see below). Throughout this response to review document your (referee review) comments are provided in regular, non-italic font text, our response comments are provided in red font (as here).

**Reviewer 1:**

**1 Summary statement**

This manuscript presents simulations from different ice sheet models showing the impact of a potential collapse of Larsen C and George VI ice shelves on the tributary glaciers feeding them. They investigate the case of a sudden and gradual collapse, and assess the impact of different model parameters (grid resolution, sliding law, ...) on the results. They show that changes in the Larsen C ice shelf have limited impact on its tributary glaciers, as this ice shelf provides a limited amount of buttressing. A collapse of George VI ice shelf on the other hand would have a much larger impact, as it provides more buttressing to its tributary glaciers and these glaciers are resting on bedrock with retrograde slopes inland, making them prone to the marine ice sheet instability.

The results presented in this manuscript are novel and interesting, showing the very different response of glaciers in two basins, in terms of grounding line retreat and contribution to sea level change. It is great to see that this study is based on three different models, however one of them is exactly state of the art, and present results largely different to the other two, so it would be great to discuss this point and conclude on the possibility (or not) to use such simple models to investigate dynamic changes of Antarctic glaciers.

Furthermore, there is not much discussion in this manuscript, just a description of the results, so it would be good to see a more substantial discussion added, including the impact of the different choices make in the model such as the sliding law used, the model resolution, and the agreement between models or between scenarios. The paper is well written and clear, except for the two tables and their captions, which are quite confusing. Below are some more detailed comments.

**2 Major comments**

I think it would be great to add “potential” in the title (“... to a potential collapse ...”), to highlight that this is just a possibility, or a future event. I think this is important given the recent collapse of the Larsen C iceberg, as it might confuse some people to talk about the collapse of Larsen C.

**We agree with the reviewer and changed the title accordingly.**

I found it confusing that the experiments are described one after the other as the text goes (new friction laws, different resolutions, ...). It would help to list all the experiments done in section 2 (maybe in 2.5 mention the additional experiments), or add a table with the list of experiments, so that the reader knows ahead of time what to expect.

**We agree and have added a table listing all perturbation experiments including sensitivity simulations as well as grid resolution to the section ‘Experimental Design’ (Section 2.5).**

In section 2.4, it is stated that the models should start with an initial state as close as possible from a steady-state. I disagree with this statement; the goal of the initialization is to get as close as possible to the conditions at a given time, including the thinning rate observed at this time. Removing this thinning/thickening rate can lead to an
underestimation/overestimation of the changes simulated, especially as this kind of signal would probably take decades to fade out. Also, how large is the flux correction applied to the models and how does it impact the simulations and the conclusions of this paper.  
The reviewer is correct that if the ice sheet is not in steady state then there should be a thinning/thickening rate after the initialisation. As the goal of this study is to tease out the contribution from ice-shelf removal to sea-level rise projections, we want an ice-sheet geometry that does not change over time. This is why we apply the synthetic mass balance to keep the geometry as close as possible to the initial geometry. To make this clearer in the manuscript we changed the first paragraph of the ‘Spin-Up’ section. It reads as follows: “Following initialisation the sheet-shelf models should be close to equilibrium if the ice sheet is close to steady state, providing dh/dt = 0. However, owing to data inconsistencies and in part a violation of this steady-state assumption this condition is not fulfilled, requiring a spin-up or relaxation simulation to reach a steady state for each model. To tease out the sea-level rise contributions from ice-shelf removal and facilitate comparison across all three ice-sheet models, the employed spin-up approach aims to keep the ice sheet geometry as close as possible to the initial geometry. “

p.10 l.2: I have a different interpretation of the Pattyn et al. (2013) paper. If steady-state grounding line positions are well captured with an internal flux condition, the paper states that “the short-time transient behavior is then incorrect” (abstract of Pattyn et al. (2013)). So such models might be less dependent to grid resolution but it does not mean that they are accurate.

We agree with the reviewer that the short-term transient behaviour of these hybrid models with an internal flux boundary condition may not be correct. However, in most of our perturbation simulations quasi steady-state is reached with PSU3D, meaning that steady-state grounding line positions should agree better between PSU3D and BISICLES after 300 years. The sentence is just stating that grid dependence is much reduced in PSU3D in comparison to BISICLES. As the Pattyn et al. (2013) paper is not the best citation for this, we have removed it from the revised manuscript.

Fig.7 shows that for some basins and variables, there is a good agreement between the PSU3D and BISICLES models for the different scenarios, while in other cases, there is a bigger difference between the two models that between the different scenarios. This should be better discussed, especially to highlight the reasons of these differences as well as the different cases. Section 3 describes these results, but there should be some discussion summarizing these findings.

We have added a paragraph to the discussion section to discuss the differences in results more in depth. It reads: “We attribute the good agreement across both models for Larsen C to the fact that the area of the marine-based sectors is limited in this domain (2.1 mm contained in marine-based sectors) due to the very mountainous bedrock topography constraining potential grounding-line retreat. This is supported by all simulations across all ice-sheet models as even under a wide range of different forcings the Larsen C embayment does not contribute more than 4.2 mm by 2300. The greater potential to initiate grounding-line retreat is presented by George VI Ice Shelf where much of the ice sheet is marine based with retrograde sloping bedrock topography (Figure 1b). As this large grounding-line retreat is only initiated in the BISICLES simulation, large differences in sea-level rise projections occur. The most likely scenario for this differing behaviour is due to the difference in the inferred basal traction coefficient fields that affects each model’s response to ice-shelf removal. PSU3D predicts much stickier bedrock conditions in the George VI embayment than BISICLES (Figure 2). These sticky bedrock conditions result in
little acceleration of the major outlet glaciers following ice-shelf breakup. This in turn means that the calving law applied to only floating ice cells cannot drive the initial retreat into the marine based sectors as the outlet glaciers do not thin sufficiently to form a floating ice tongue. In contrast in the RCP8.5 BISICLES simulation for George VI, speed-up in response to ice-shelf breakup leads to enhanced dynamic thinning of the main outlet glaciers. This thinning in conjunction with the calving law drives the calving front into the marine-based sectors where further retreat is initiated by a combination of the marine ice-sheet instability and the meltwater driven calving law, resulting in the simulated much higher sea-level rise projections.”

Overall, there is no real discussion, just a description of the results. A proper discussion should include the current limitations of the models and future possible improvements, the impact of the different models compared to other parameters, such as the sliding law employed, the scenario chosen, or the bedrock used, with references to previous studies. We have added a paragraph to section 3.3 that discusses and highlights the model limitation, key parameter uncertainties and improvements for future studies. It reads: “In addition, our experiments show that for simulations of grounding-line motion in response to ice-shelf breakup sheet-shelf models are necessary. The simple model BAS-APISM fails to reproduce the results of the sheet-shelf models due to the simplified physics. Even across sheet-shelf models differences in model physics, model initialisation, calving law implementation and other numerics (e.g. meshing) can lead to substantially different projections under the same forcing (Figure A5). Sea-level rise projections are most sensitive to the choice of sliding law and bedrock geometry. The peninsula is not the only region where these parameters highly affect decadal to centennial sea-level rise projections as similar conclusions were drawn from modelling of outlet glaciers in the Amundsen Sea embayment (Nias et al., 2018). The wide range of sea-level rise responses to different forcing parameters underlines the need for perturbed ensembles to explore key parameter uncertainties (e.g. basal sliding law) for sea-level rise projections in greater detail for the peninsula region. Owing to the increase in computer power these type of ensemble projections have become feasible at the regional (e.g. Nias et al., 2016) and continental scale (e.g. DeConto and Pollard, 2016).

3 Specific comments
p.1 l.1: “past several”: be more precise
changed to “past five decades”
p.1 l.13: “northerly limit”: it would be great to explain this limit in a few words
we added “… determined by the -9°C mean annual isotherm…”
Fig.1: “meters above sea level” is a bit confusing as all elevations are negative, maybe simply saying “in meters” would be enough. Also mention that the colorbar is truncated at 0, and maybe add the highest elevation in this area. The black polygons are not clear and can be confused with the grounding line position, consider using a different color or thick lines.
We have changed the text and figure accordingly. Black polygon lines have been made thicker and we simply state now “…elevations below sea level in meters”.
p.2 l.7: mention that happens on downward sloping bedrock elevation inland (not just on all marine based sectors)
We added “…and retrograde sloping bedrock topography…”
p.2 l.9: remove “state-of-the-art” as I am not sure that the BAS-APISM model can be considered to be a state-of-the-art model (“simulates ice flow by solving the simplest permissible force basal approximation” p.3 l.7)

Removed

p.2 l.10: same as the title: add that you are talking about a potential collapse

Done

p.3 l.10: “SIA is not valid at the grounding line”, the problem here is rather that SIA is not valid on floating ice shelves and fast flowing ice streams.

Changed to: “As the SIA is not valid for floating ice shelves, ...”

p.3 l.16: “in assumed” → “is assumed”

Changed

p.3 l.34: Add sentences in the three model descriptions about the grid resolution (and grid resolution at the grounding line) employed in these three models.

We have added this information to the table where all simulations are listed.

p.4 Eq.1: What basal conditions (friction) is used for the BAS-APISM model?

We added a sentence specifying that due to the linearisation there is no need to specify whether or not basal sliding is occurring. It reads: “Due to the linearisation of the evolution equations in BAS-APISM, there is no need to specify whether or not basal sliding is occurring. All rates are determined by the ice flux which is directly derived from the data.”

p.5 l.20: What is R exactly and how does it relate to the temperature in a few words?

We added: “This formula scales surface melt exponentially with mean DJF near surface temperatures ...”

p.5 l.24-25: How is this done (in a sentence or two)? Some technical explanations are missing.

We have added a sentence saying: “This is accomplished through the computation of balance fluxes.”

p.6 l.18: ALBMAP is quite old, why not use the new BEDMAP2 or Huss and Farinotti, (2014) data for all the models?

The difference in ice volume and bedrock topography between ALBMAP and BEDMAP2 for the Antarctic Peninsula is rather small (<15%) and the Huss and Farinotti (2014) dataset is only available for the Larsen C domain as it does not cover the southern part of the peninsula. To gauge the importance of differences in bedrock topography, we carried out the sensitivity simulation with BISICLES for the Larsen C domain. As the difference between BEDMAP2 and the Huss and Farinotti (2014) dataset is large (“100% in ice volume below sea level), large differences propagate into the magnitude of the sea-level rise projections.

p.6 l.23: As mentioned above, do you really want the simulations to start from a steady-state? Or from the current thinning/thickening rate? Why not correct this by adding the rate of thickness change instead of assuming that it is 0? And by the way, I don’t agree that “After initialization, the sheet-shelf models should be in equilibrium”. The models should represent the actual ice sheet state at the time captured by the initialization, so if the ice sheets where thinning, the initialization should capture and reproduce this initial thinning.

p.6 l.28: Adding this flux correction is fine, but you should show how large it is, and how large it is compared to the actual surface mass balance. Also, how different are the results if you don’t include it? What are the impacts on the simulations?

See reply above. In brief, in order to really tease out the contributions that come from ice-shelf removal alone, we desire all other signals to be as close as possible to zero. This is
why we apply the synthetic mass balance to keep the ice-sheet as close as possible to its initial geometry. Of course the results of our simulations would be different without the additional synthetic surface mass balance forcing, but comparing our projections with and without this flux term is not the goal of this study.

p.7 Fig.2: Why not show the BAS-APISM model here? I have a hard time understanding what the basal boundary condition of this model is. Also should be “Black lines denote ...”

Due to the linearization of the evolution equation there is no need to specify whether or not basal sliding is occurring and balance fluxes are used to initialise the model.

p.8 l.3: What resolutions are used? The list of experiments with their characteristics should be better detailed in the text.

We have added a table with all simulations and their respective resolution to section 2.5.

p.9 l.12: Over what period does this change happens?
We added: “... averaged over 300 years”

p.9 l.14-19: The initial conditions (ice velocity, thickness, elevation, rigidity, ...) also have an impact on the evolution of the glacier, as well as the numerical parameters (grid resolution, ...).

We added: “This discrepancy between the sheet-shelf models may be attributed to a combination of differences in initialisation and that PSU3D is not as close to steady-state as BISICLES following initialisation and spin-up.”

p.9 l.14-19: What about the BAS-APISM model?
As there is no time-dependent grounding-line migration after the initial perturbation, we focus on the sheet shelf models, but state at the end of the paragraph that BAS-APISM projects similar magnitudes of sea-level rise, but the spatial thinning pattern is very different to the sheet-shelf models.

p.10 Fig.4: Should be: “Upper panels (a, b) show ...”, same for “Lower panels ...”

Changed

p.10 l.2: As mentioned above, the Pattyn et al. (2013) paper says that “the short-time transient behavior is then incorrect” for grounding line evolution captured with internal flux conditions.

See reply above. We have removed the Pattyn et al. (2013) citation.

p.11 Fig.5: Should be: “Black lines denote ...”. Same for caption in Fig.6.

Changed

p.15 l.3: “A consequence of this is ...” → “A consequence is ...”

Changed

p.15 l.23: “most of grounding-line retreat” → “most of the grounding-line retreat”

Changed

Tables 1 and 2: the tables and their captions are quite confusing. Especially as all numbers reflect different time periods, and some variables are not standard (e.g., dGt/dt for mass change rate). Also why not use the same order as Fig.6 (BAS-APISM left, ...).

As suggested by the second reviewer, we have moved the tables to the Supplementary material as they disrupted the flow of the paper. We also changed the dGt/dt to the correct dM/dt and the respective units (if not unitless) are provided in the table caption.

We also changed the order of the columns to follow the order of Figures 6 and 8 for Experiment 1 and Experiment 2, respectively. Moreover, we now present a separate table for George VI and Larsen C basins and added the Coulomb sliding BISICLES simulation for Experiment 1 to Table S1.

Table 2: Fig.A7 shows larger grounding line retreat for many glaciers (GeoIII, GeoIV, ...) with the Coulomb friction law, which does not seemed to be reflected in this table. But as I just
mentioned above, I am quite confused by this table. I would also expect this increased grounding line retreat to transfer in more mass change for the Coulomb case. It would be simpler to have both BISICLES cases next to each other.

**Due to the confusing layout, the reviewer confused Experiments 1 and 2 here. They do show larger grounding-line retreat but only in comparison to other simulations from Experiment 1, but not in comparison to Experiment 2. We added the Coulomb sliding BISICLES simulation for Experiment 1 to Table S1 to make this clearer.**

p.18: As mentioned previously, there is not much discussion, just a description of the results. See reply above.

p.19 l.6: “vulnerability of ice-shelf …” → “vulnerability to ice-shelf ..”

**Changed**

Fig.A1: Y-axis label should be “Temp. bias” not “Temp.”. Caption should detail bias which two quantities.

Fig.A2: Same as Fig.A1

**Changed and added “…in relation to ERA-Interim.”**

Fig. A6: Caption should be “Upper panels (a,b) show …”. Same for “Lower panels …”

**Changed**

Fig. A7: Simulations with Coulomb friction show a larger retreat, which is not captured in Table 2.

**It is captured. See reply above.**

**Reviewer 2:**

General comments
April 12, 2018

This paper from Clemens Schannwell and his colleagues investigates, in a timely manner, the response of the Antarctic Peninsula glaciers to a collapse of the Larsen C and Georges VI ice shelves. They use three types of numerical models of different complexity applied to two main experiments, supplemented by secondary experiments. Experiment 1 starts without ice shelves, as if an ice shelf collapse had already occurred, Experiment 2 starts with the current geometry and use a calving law and potentially leads to ice shelf collapse, depending on future scenarios, which are either RCP4.5 or RCP8.5. The secondary experiments help to quantify uncertainties, and are built upon Experiment 2 to which was added mild or strong sub-shelf melting, and a last experiment use another dataset for ice geometry (the one of Huss and Farinotti 2014) instead of the classical Bedmap2 dataset used elsewhere in the study. All those experiments are simulated from today to 2300.

I find this study very interesting and I think this can be published with minor revisions. The fact of applying different types of ice sheet models, having not only different physics for time evolutive simulations but also different approaches for building the initial spin-up (inversion + relaxation), to the same case of study is not easy but it makes the results more robust. The paper is globally well written apart from some details on which you will have specific comments below. The description of the methods is quite clear, even though it lacks the definition of Glen’s flow law from which the authors could introduce the enhancing factor, which should be defined clearly.

I first have a couple of minor concerns:
- The Spin-up for BISICLES at a 1000m resolution looks odd from Figure3, the results doesn’t seem to converge with the resolution (dvdt at 0 very rapidly for 4000, 2000 and 500m resolutions, but quite different for 1000m). Did you, by any chance, accidently shift, say, the
colors for 4000m and 1000m?? If not, could you make a few comments on that in the paper.

We did not expect convergence in the spin-up simulations by increasing the mesh resolution. These simulations all use a synthetic surface mass balance that is derived from their respective model grids after one timestep. In some of the simulations, the model drift and the remaining thinning/thickening signal following initialisation may not be as well captured after one timestep as in others (e.g. 2000 m vs. 1000 m BISICLES). In addition, the initialisations were performed also on different grids (1 km for BISICLES and 5 km for PSU3D). All in all, these factors most likely lead to the slightly different dV/dt patterns that are shown in Figure 3. Considering that steady-states with real world geometries are difficult to achieve, we are satisfied with how close they are to steady state after relaxation. PUS3D could not be run at higher resolution as it became unstable at resolutions of < 1000 m. Therefore, we chose 1000 m.

- I was not always sure about the type of SMB that you applied, for the spin-up but also for the experiments. You introduce the Albmap SMB but in the inversion process, not in the spin-up neither in the description of transients. Make it more clear in the text.

We have added a sentence to section 2.4 that clarifies that we use the synthetic mass balance for all experiments. It reads: “This synthetic mass balance is applied in all spin-up and perturbation simulations.”

- Could you change the time origin in the evolutive plots to be 2000 instead of 0?

Changed accordingly

- Could you mention that sub-shelf melting is always 0 (if I understood correctly), apart from your two additional experiments.

We added a sentence to section 2.5. to clarify this. It reads: “Moreover, ocean melting is set to zero in the perturbation experiments unless stated otherwise.”

- I would be glad if you could indicate the position of the calving front in your maps of Experiment2 results, for 2100 and 2300 for instance, or maybe, if it’s more easy, indicate the year of collapse in Figure7. This would strongly help the understanding of ice dynamics differences between Exp1 and Exp2.

We think that adding the calving front to Figure 8 at these two timesteps would clutter up the Figure too much. Moreover, the calving front in 2300 is very close to the grounding-line that is drawn in Figure 8 anyway. Rather than visualise the calving front with lines in Figure 8, we find the ice-shelf area loss plots (Figure 7e, f) more informative as the evolution of ice-shelf retreat can be tracked better over time. In addition to these plots, we added a sentence that states that once the ice shelf has collapsed, grounding-line and calving front are almost in identical locations.

- I would be in favor of adding a table to summarise all the experiments, including the main exp1 and Exp2 but also the three others.

We have added a table listing all experiment and the resolutions at which they were run to section 2.5.

- I would also be in favor of adding those results to Table2, and put the two tables in the supplementary, to help the reading and understanding of what has been done.

Yes, we moved the tables to the Supplementary as they disrupted the flow of the paper. We also changed the dGt/dt to the correct dM/dt and the respective units (if not unitless) are provided in the table caption. We also changed the order of the columns to follow the order of Figures 6 and 8 for Experiment 1 and Experiment 2 respectively. Moreover, we now present a separate table for George VI and Larsen C basins and added the Coulomb sliding BISICLES simulation for Experiment 1 to Table S1.
Some assertions are not always correct in the reading of the results (see below)
The rest of my review is a series of specific comments and recommendations, which would like to be followed as well.

Specific comments
Page 1
l17: Could you mention those other mechanisms?
We added “… such as ice-shelf thinning, fracturing, and weakening of shear margins …”
l18: Could you add a word like "slightly" just before increased? This is at least what I understand from the Jansen et al., 2015 study
Done
Page 2
Figure 1:
- The Y label should be "elevation [m a.s.l]"
- In the caption, "localities mentioned in the text"
- In the caption, remove "below sea level"
- In the caption, replace "Black polygons..." by something like "The grounded part of the ice sheet only is represented"
We have changed to “localities in the text” and followed the suggestions from reviewer 1.
Black polygon lines have been made thicker and we simply state now “...elevations below sea level in meters”.
l8: "a tendency...": Here the way this instability works doesn’t appear clearly. Nowhere there is written that you have deepening of the bedrock towards the interior, which is a necessary condition (at the necessary condition that bedrock is below sea level) to a MISI. Be more precise please.
We added “…and retrograde sloping bedrock topography…”
Page 3
l10: Why is the SIA not valid at the grounding line? could you mention the reason or/and add a citation here?
We have added a citation to (Hutter, 1983)
l21: The way this is said, it is not clear whether the condition is imposed at the grounding line, to me at least... Could you rephrase.
We have added “… is employed at the grounding line.”
Page 4
l11: Is there a reason to take 0.5 specifically? Tsai et al., advises f<0.6, Brondex et al., takes 0.5. Could you make a few comments on that.
Most ice-sheet modelling studies have used a value of f=0.5 (see Asay-Davis et al. 2016, Brondex et al. 2017, Nias et al. 2018). To keep in line with this, we chose the same value for our simulations.
Page 5:
l9: So the criterion in Bisicles is Height surface crevasse + Height basal crevasse = ice surface? this is not clear to me
We have rewritten to read: “...reaches the distance from ice surface to the waterline.”
l12: Do you need a capital H in historical?
Changed to lower case.
l29: You should have defined this enhancement factor before reaching this part. It is worth to detail the Glen’s flow law equation somewhere above, from which you can easily define the enhancement factor.
Added to the section 2.1.
I am glad you showed Figure A3 (Hum, this figure reminds me Belgium...)

We added a sentence to acknowledge this. It reads: “The layout was inspired by Berger et al. (2016).”

Something is wrong here, or is this a typo?

We added “...for the inversion simulation.” We then recompute the basal drag coefficient field from the inversion (linear sliding) for the other sliding laws used in the perturbation experiments.

You used SMB for the spin-up only (and also the transient for, could you be more accurate here

This was ambiguous. We removed surface mass balance here and added a sentence to section 2.4 that clarifies that we use the synthetic mass balance for all experiments. It reads: “This synthetic mass balance is applied in all spin-up and perturbation simulations.”

Figure 2: Is that the PSU3D grid that we can distinguish in Figure 2? Why is that so?

We do not know what the reviewer means by this. No grids are shown in Figure 2. Only the outline of our model domain (black polygon) is visible.

Changed.

This is not clear what you took for SMB in Experiment 1?

We added a sentence to section 2.4 that clarifies that we use the synthetic mass balance for all experiments. It reads: “This synthetic mass balance is applied in all spin-up and perturbation simulations.”

Isn’t that curious that the 1000m resolution results for BISICLES are outlying compared to the others? I would have expected the results to converge when getting closer to 500m resolution, but it is not the case here. Could you discuss that?

The solution of PSU3D is not really converging. The model can’t be applied at a lower resolution? Could you add few comments on that if you find it relevant.

We did not expect convergence in the spin-up simulations by increasing the mesh resolution. These simulations all use a synthetic surface mass balance that is derived from their respective model grids after one timestep. In some of the simulations, the model drift and the remaining thinning/thickening signal following initialisation may not be as well captured after one timestep as in others (e.g. 2000 m vs. 1000 m BISICLES). In addition, the initialisations were performed also on different grids (1 km for BISICLES and 5 km for PSU3D). All in all, these factors most likely lead to the slightly different dV/dt patterns that are shown in Figure 3. Considering that steady-states with real world geometries are difficult to achieve, we are satisfied with how close they are to steady state after relaxation. PSU3D could not be run at higher resolution as it became unstable at resolutions of < 1000 m. Therefore, we chose 1000 m.

Deleted.

Results and discussion

Sea-level rise by 2100?

For clarity we added: “...by 2300.”
I17: The differences in terms of sea level response may be due to those large differences that you have between friction coefficients fields?

We have rewritten this sentence. It reads: "This discrepancy between the sheet-shelf models may be attributed to a combination of differences in initialisation, inferred basal traction fields, and that PSU3D is not as close to steady-state as BISICLES following initialisation and spin-up."

I18: Could you maybe detail the relevant specific differences?

We have extended this paragraph to accommodate this. It reads: "Such a response has been previously attributed to differences in the underlying model physics (L1L2, A-HySSA). Using synthetic geometries, A-HySSA models have shown to be more sensitive to grounding-line advance as well as retreat. These differences are most likely caused by the neglecting of vertical shearing terms in the pure membrane ice-sheet models (Pattyn et al., 2013)."

Page 10

Figure 4: Could you start your time scale at 2000?

Changed.

I1: where do we see the dependence to grid resolution in Figure A4? This is rather observed in Figure A6. Changed.

And according to Figure A6, there is also a sea level contribution dependency to grid resolution in PSU3D. Moreover, this is true that this dependency is small for Georges VI (not absent though) and comparable to BISICLES for Larsen C. Could you rephrase here.

We rephrased to: "... much reduced ..."

I4: you definitely refer to Figure A6

Yes, we changed it accordingly.

Page 11

Figure 5: It seems that the 2000 grounding line is slightly different between PSU3D and BISICLES. The differences are difficult to quantify, so could you maybe write down somewhere the maximum difference between initial grounding lines for the two models?

We state in section 3.2 that the effect of the more advanced grounding-line position in PSU3D for the Larsen C domain accounts for a sea-level equivalent of 0.28 mm. We find this number more informative than a maximum difference in grounding-line position and therefore would like to keep it.

I10: A necessary condition to have a MISI is a retrograde bed slope, insofar as you have a marine based basin as well. You thus need to replace "mostly marine-based outlet" by "retrograde bed slope something..."

Changed

I13: Could you discuss this a bit more. There is this paper from Gudmundsson et al., in 2012 and Gudmundsson in 2013 about the buttressing provided by an ice shelf to its upstream glacier as a function of the grounding line gate width...

This is a good point. We have extended the paragraph to discuss this now. It reads: "These findings suggest that stabilising forces such as basal and lateral drag may provide enough resistance for the ice sheet in western Palmer Land to remain in a stable configuration following the initial response to ice-shelf collapse. This is supported by earlier modelling studies with idealised geometries, showing that the magnitude of grounding-line retreat is a function of the retrograde sloping channel width (Gudmundsson et al., 2012, Gudmundsson et al., 2013). The smaller the channel width, the less retreat was simulated (Gudmundsson et al., 2012). Considering the small size of the drainage basins in the
peninsula region with channel widths <30 km, the remaining lateral buttressing from shear margins likely impedes any runaway grounding-line retreat.”

Page12
I3: "dependent"
Fixed.
I7: Remove "fixed calving front simulation, immediate shelf-collapse scenario" and keep "Experiment 1"
Changed.
I10: Remove "just"
Removed.
I10: "the larger" -> "the largest"
We think “the larger” is correct.
Page13
Figure7: Time between 2000 and 2300
Changed
I1: "projections ... agree well": this is not really what I see in Figure7a, where the two models may agree for the first 50 to 70 years, but not really for the rest of the simulations. Could you rephrase?
We added “...reasonably well ...”
I4: "BISICLES projects no slr for RCP4.5": more correct would be to say "small" or "limited" instead of "no", especially for Larsen C
Changed to “little”
Page14
I1: "Both sheet-shelf models project similar sea-level rise by the mid 22nd century in Experiment 2": Again, I don’t agree with this sentence, after 250 years Larsen C ice loss is 0.25 and 0.6 for BISICLES4.5 and PSU3D4.5, and this is not the only example where I find differences where you write the opposite (see above). You should rewrite here.
Sorry this statement was meant for the George VI embayment. We have added a qualifier at the end of the sentence: “... for the George VI domain...” We also meant 2150 with “the mid 22nd century”. To avoid any confusion, we changed this phrase to 2150.
I2: What do you mean by "forced back”? Does it simply mean that the grounding line retreat? Could you rephrase?
Yes. We changed this to read: “...grounding lines retreat further back into ...”
I3: "because a fixed calving front": Here I don’t understand, the fact of having a fixed calving front does not prevent the retreat of the grounding line. You need to rephrase.
Yes, we have rephrased it. After ice-shelf collapse grounding line and calving front are in almost identical locations. To highlight this, we added: “After ice-shelf collapse, grounding line and calving front for all drainage basins are almost in identical locations.”
I1 to I14: For this paragraph, this is not cristal clear to me if you talk about Georges VI or Larsen C ice shelf. Can you make the text more clear please.
Yes, it was not very clear. We rewrote sections of the paragraph and also added a paragraph to discuss the difference in projections across the models.
I25: Don’t understand this sentence. you say that your model show a strong dependence to what? Calving criteria or sub-shelf melting
We rephrased this to read: “...in other words, it is ice-shelf break-up in combination with the calving criteria that dominates our results.”
I3: Ok, this is another experiment. I recommend to add a table to summarize all the experiments.

    Done. See above.

I8: five more drainage basins, means not the LarI to LarV and Geol to GeoV? could you indicate in a figure which are the supplementary basins that you accounted for? Maybe put it into Figure8?

    Apologies this was ambiguous. We indeed mean the basins LarI to LarV and Geol to GeoV. This sentence was changed to improve clarity. It reads: “To further assess the impact of ice-shelf break-up, five drainage basins from the Larsen C embayment (LarI-LarV, Figure 8) and George VI embayment (Geol-GeoV, Figure 8) were selected for additional analysis.”

Page17

Table1: What did you put in parenthesis from the dGL and dGt/dt columns? Does it correspond to the year you had the maximum speed up? You need to write it down then.

Table1 and Table2: Would you like to move those 2 tables in the Supplementary? I have the feeling that it affects the reading of the paper...

    Yes, we moved the tables to the Supplementary as they disrupted the flow of the paper. We also changed the dGt/dt to the correct dM/dt and the respective units (if not unitless) are provided in table caption. We also changed the order of the columns to follow the order of Figures 6 and 8 for Experiment 1 and Experiment 2 respectively. Moreover, we now present a separate table for George VI and Larsen C basins and added the Coulomb sliding BISICLES simulation for Experiment 1 to Table S1.

Page19

I4: You definitely need to show your results with the Fuss and Farinotti geometry

    The Huss and Farinotti results have been added to Figure 4

Supplementary

Figure A3: Could you explain why you chose $\lambda_c = 10^{-1}$? It doesn’t seem that obvious looking at A3c. Stupid question maybe, why is there a jump between $10^{-1}$ and $10^1$ (I mean no $10^0$ appearing)?

    Apologies. The exponent 0 was missing. This is now fixed. We chose $10^{-1}$ because we wanted to make sure that we are close to the kink of the L but still on the lower branch. $10^0$ was too close to the kink in our opinion.

FigureA6: Time origin should be 2000

    Changed accordingly.

    We amend the following sentence to the manuscript acknowledgements, to read: ‘We thank the editor Olivier Gagliardini, Lionel Favier, and an anonymous reviewer for comments which improved the manuscript.’.