



1 **Estimation of soil properties by coupled inversion of electrical resistance, temperature, and**
2 **moisture content data**

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17 **Abstract**

18 Studies indicate greenhouse gas emissions following permafrost thaw will amplify current rates of
19 atmospheric warming, a process referred to as the permafrost carbon feedback (PCF). However,
20 large uncertainties exist regarding the timing and magnitude of the PCF, in part due to uncertainties
21 associated with subsurface permafrost parameterization and structure. Development of robust
22 parameter estimation methods for permafrost-rich soils is becoming urgent under accelerated
23 warming of the Arctic. Improved parameterization of the subsurface properties in land system
24 models would lead to improved predictions and reduction of modeling uncertainty. In this work
25 we set the groundwork for future parameter estimation (PE) studies by developing and evaluating
26 a joint PE framework that estimates soil properties from time-series of soil temperature, moisture,
27 and electrical resistance measurements. The framework utilizes the PEST (Model Independent
28 Parameter Estimation and Uncertainty Analysis) toolbox and coupled hydro-thermal-geophysical
29 modeling. We test the framework against synthetic data, providing a proof-of-concept for the
30 approach. We use specified subsurface parameters and coupled models to setup a synthetic state,



31 perturb the parameters, then verify that our PE framework is able to recover the parameters and
32 synthetic state. To evaluate the accuracy and robustness of the approach we perform multiple tests
33 for a perturbed set of initial starting parameter combinations. In addition, we evaluate the relative
34 worth of including various types and amount of data needed to improve predictions. The results of
35 the PE tests suggest that using data from multiple observational datasets improves the accuracy of
36 the estimated parameters.

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39 **1. Introduction**

40 Subsurface soil property parametrization contributes to a wide uncertainty range in projected
41 active layer depth and in simulated permafrost distribution in the Northern Hemisphere when
42 predicted using Land System Models (LSM) (Koven et al., 2015; Harp et al., 2016). Reduction of
43 this uncertainty is becoming urgent with recent accelerated thawing of permafrost (Biskaborn et
44 al., 2019). Warming permafrost leads to increase infrastructure maintenance costs (Hjort et al.,
45 2018), has a positive feedback on global climate change (McGuire et al., 2018), and increases the
46 probability of the potential hazards for human health (Schuster et al., 2018). Better subsurface soil
47 property parametrizations in LSMs requires the development of methods that can robustly estimate
48 these soil properties including porosity and thermal conductivity of peat and mineral layers.

49 Direct measurements of subsurface soil properties are labor intensive, destructive, and not always
50 feasible (Smith and Tice, 1988; Kern, 1994; Boike and Roth, 1997; Yoshikawa et al., 2004). While
51 soil sample analysis can provide critical information on soil properties at a fine scale, this
52 information is limited to sparsely sampled locations. Multiple methods used in the laboratory to
53 measure soil properties by using soil cores extracted from the field site are well summarized by
54 Nicolsky et al., (2009), but logistical and economic burden typically do not allow these
55 measurements to be made in the field. Inverse modeling serves as an alternative approach to
56 recover soil properties using a combination of indirect measurements and physics-based numerical
57 models.

58 Different inverse modeling frameworks have been developed to estimate soil thermal properties
59 using physical-based models and time-series of soil moisture, temperature and/or geophysical data.
60 Many use a heat equation without phase change (Beck et al., 1985; Allifanov et al., 1996). More
61 recent works include phase change, which is an important component of the energy balance in



62 permafrost-affected soils (e.g. Nicolsky et al., 2007; 2009, Tran et al., 2017). Nicolsky et al.,
63 (2007; 2009) used an optimization based inverse method and a variational data assimilation
64 method to estimate soil properties. Harp et al., (2016) used an ensemble-based method to evaluate
65 the uncertainty of projections of permafrost conditions in a warming climate due to uncertainty in
66 subsurface properties. Atchley et al., (2015) used data calibration to estimate hydrothermal
67 properties of soils. All these methods used ground temperature timeseries alone to estimate soil
68 properties through their role in modulating heat fluxes. Moreover, all these methods utilized 1D
69 soil columns and therefore assume 1D soil structure.

70 Recently, Tran et al., (2017) used a coupled hydrological–thermal–geophysical modeling approach
71 to estimate soil organic content. The approach was based on coupling the 1D Community Land
72 Model (CLM4.5; Oleson et al., 2013) that simulates surface–subsurface water, heat and energy
73 exchange and the 2D Boundless Electrical Resistivity Tomography (BERT) forward model
74 (Rücker et al., 2006). The simulated 1D profiles of the subsurface temperature, liquid water
75 content and ice content from CLM model were explicitly linked to soil electrical resistivities via
76 petrophysical relationships and then to soil electrical resistances using the BERT forward model.
77 Here we modify and extend this approach to 2D by using the Advanced Terrestrial Simulator
78 (ATS) model, which was specifically developed to study fine-scale hydrothermal processes of
79 permafrost-affected soils. In addition, instead of estimating organic content of the soil as in Tran
80 et al., (2017), we estimate properties of peat (organic) and mineral layers across a 2D transect
81 within polygonal tundra.

82 Modeling the full, continuous 2D transect allows us to simulate lateral hydro-thermal fluxes not
83 possible with individual 1D columns known to be important in polygonal tundra (Abolt et al, 2018,
84 Liljedahl et al, 2016). At each grid cell in the transect, a unique state develops during the ATS
85 simulation (temperature, saturation, etc.) that is then used to calculate heterogeneous electrical
86 resistivities via petrophysical relations. This allows more realistic simulated electrical resistances
87 that include the effects of lateral hydrothermal connectivity within the transect.

88 Through this approach, we develop a parameter estimation (PE) framework that is able to estimate
89 subsurface properties in permafrost-affected soils through joint inversion of hydrothermal and
90 geophysical measurements. Our main objective then is to evaluate which types and number of
91 measurements are necessary to constrain the inversion to yield a robust and accurate prediction of
92 subsurface properties. The method jointly inverts based on matching multiple types of

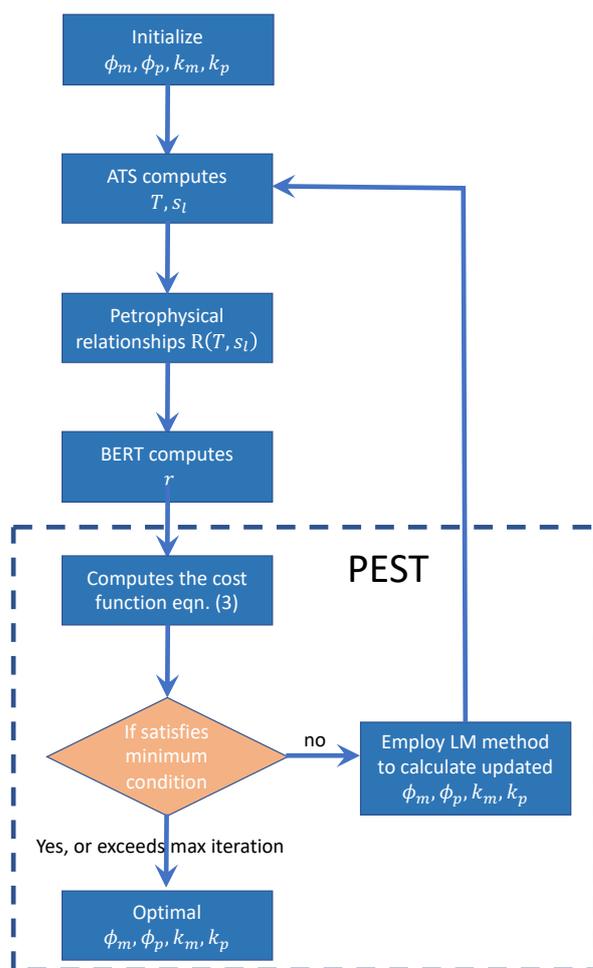


93 measurements (temperature, saturation, and electrical resistivity) using a forward modeling
94 framework that couples a state-of-the-art hydrothermal permafrost simulator with an electrical
95 resistance simulator. We progressively test the accuracy and robustness of the method using a
96 series of synthetic problems by: 1) increasing the complexity of the meteorological data used to
97 drive the coupled thermo-hydro-geophysical model and 2) testing the inclusion of individual and
98 combinations of several available measurement types on the accuracy and repeatability of
99 inversions. We further used findings from this study to suggest how data should be collected to
100 improve the accuracy of the estimated soil properties and to optimize total number measurements
101 needed to make a robust subsurface PE. The results of this work can be used to better understand
102 uncertainties associated with subsurface soil property estimation. In addition, the approach can be
103 used to inform field campaigns to ensure that sufficient measurements are collected to allow soil
104 property estimation at a desired accuracy.

105

106 **2. Methods**

107 We estimate effective soil properties for peat and mineral layers of a 2D transect within polygonal
108 tundra. Our PE approach is summarized in Figure 1. We utilized the Advanced Terrestrial
109 Simulator model version 0.86 (ATS), a fully 3D-capable coupled groundwater flow and heat
110 transport model representing the soil physics needed to capture permafrost dynamics, including
111 ice, air, and liquid saturation, flow of unfrozen water in the presence of phase change, and non-
112 homogeneous soil layering (Painter et al., 2016). We sequentially coupled ATS with the
113 Boundless Electrical Resistivity Tomography (BERT) model (Rücker et al., 2006), which we run
114 in forward mode to compute ERT survey resistance values based on soil resistivities calculated
115 using ATS output (temperatures, saturations, etc.) and petrophysical relations. The forward mode
116 of BERT solves Poisson's equation using the finite-element method to calculate ERT survey
117 resistances in a two-dimensional tomography corresponding to the cross section of the ice-wedge
118 polygonal tundra site.



119
 120 **Figure 1.** Schematics of the parameter estimation algorithm.

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122 **2.1 Synthetic Model**

123 To setup the synthetic model, we used digital elevation data of a transect through ice-wedge
 124 polygonal tundra at the Barrow Environmental Observatory (BEO), at Utqiagvik, Alaska. The
 125 mesh shown on Figure 2A represents the cross-section of the polygonal tundra. Thickness of the
 126 peat (organic) layer corresponds to observations at the site, with a thick peat layer on the sides
 127 (troughs) and thinner in the middle of the low center polygon. A mineral layer was assigned below
 128 the peat layer across the transect. We initially designated six synthetic observation (temperature
 129 and soil moisture measurement) locations within the active layer thickness (ALT) similar to the
 130 sensor setup at the site (Dafflon et al., 2017). Then we added 4 more synthetic observation



131 locations below the ALT (Figure 2B) to better understand the effect of their inclusion on PE
132 accuracy and robustness. All observation locations are represented as stars on Figure 2A
133 corresponding to the locations of the collected temperature and soil moisture timeseries. The
134 temperature and soil moisture timeseries were observed at depth 5, 20, 60, and 80 cm below the
135 surface. The overall depth of the modeling domain is 45 m. We set the bottom boundary to a
136 constant temperature of $T=263.55\text{K}$, and closed (zero heat and mass flux) boundary conditions on
137 the vertical sides. The required steps to establish a water table in permafrost soils in the ATS
138 model have been documented in Atchley et al., (2015) and Jafarov et al., (2018). A seepage face
139 was imposed at 4 cm below the surface on each side of the domain to allow drainage through
140 connected trough networks and preventing water from pooling at the surface, as is typical of
141 partially degraded polygonal ground (Liljedahl et al, 2016). We use two types of meteorological
142 datasets as surface boundary condition drivers for the ATS model: simplified (sinusoidal air
143 temperature, constant precipitation, and constant radiative forcing) and actual weather data from
144 the BEO site. The actual meteorological data were collected starting on January 1, 2015 and
145 includes air temperature, rain and snow precipitation, humidity, long and shortwave radiation and
146 wind speed. We present ground temperatures simulated for the synthetic model run with actual
147 meteorological data in Figure 2B, where the linear white region indicates the ALT within the
148 transect (i.e., 0°C). The deepest ALT is in the middle of the transect (42 cm) and shallowest on
149 the sides (35 cm). In addition, In Figure 3 we present corresponding liquid-water and ice saturation
150 for the synthetic model run at different times of the year.

151 ATS uses the designated porosities and thermal conductivities $\{\phi, k\}$ of peat and mineral soil layer
152 to compute temperature (T) and liquid-water saturation (s_l) designated as the synthetic truth. To
153 calculate thermal conductivities of the air-water-ice-soil mixture, the ATS model interpolates
154 between saturated frozen, saturated unfrozen, and fully dry states (Painter et al., 2016) where the
155 thermal conductivities of each end-member state is determined by the thermal conductivity of the
156 components (soil grains, air, water, or liquid) weighted by the relative abundance of each
157 component in the cell (Johansen, 1977; Peters-Lidard et al, 1998; Atchley et al., 2015). Standard
158 empirical fits are used for the internal energy of each component of the air-water-ice-soil mixture.
159 The corresponding equation used to calculate saturated, frozen thermal conductivity ($\kappa_{sat,f}$) has
160 the following form:

$$161 \quad \kappa_{sat,f} = \kappa_{sat,uf} \cdot \kappa_i^\phi \cdot \kappa_w^{-\phi}, \quad (1)$$

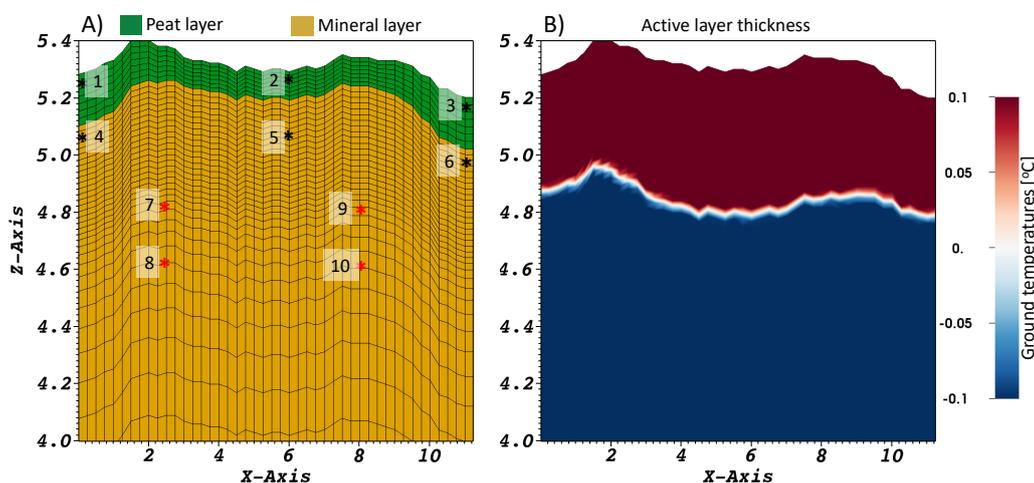


162 where $\kappa_{sat,uf}$, κ_i , κ_w are thermal conductivities for saturated unfrozen, ice, and liquid water,
 163 respectively, and ϕ is porosity.

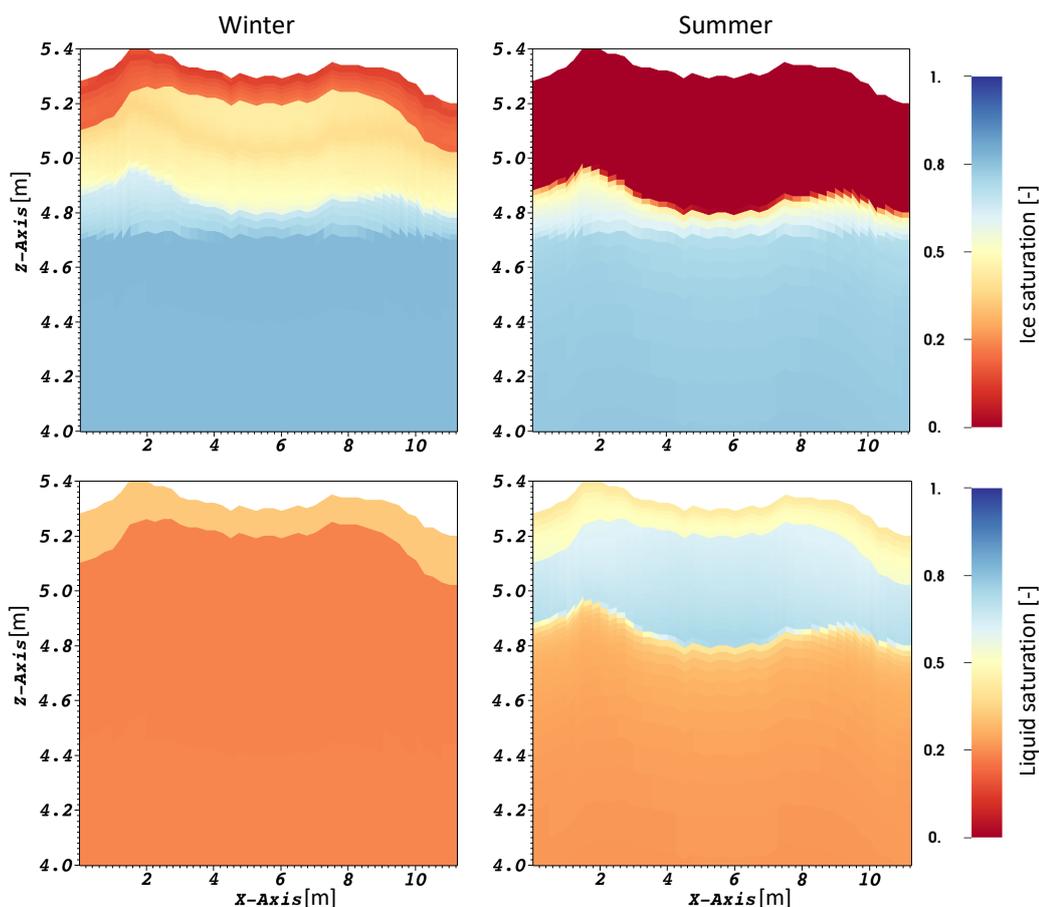
164 We sequentially couple the ATS and BERT numerical models via petrophysical relationships used
 165 by Tran et al., (2017). In that approach, the electrical conductivity is determined as a function of
 166 temperature and liquid water saturation:

$$167 \quad R(T, s_l) = 1/(\phi^d [s_l^n \sigma_w + (\phi^{-d} - 1)\sigma_s] \cdot [1 + c(T - 25)]), \quad (2)$$

168 where $R(T, s_l)$ is the electrical resistivity, σ_w and σ_s are the electrical conductivities of water and
 169 soil/sediments, respectively, n is a saturation index, d is a cementation index, and c is a
 170 temperature compensation factor accounting for deviations from $T = 25^\circ C$. Calculated electrical
 171 resistivities get passed to the BERT model which computes electrical resistances (r) such as
 172 measured during an ERT survey. In this study we assume all constants used in equation (2) are
 173 known (see Tran et al., 2017) and focus on the uncertainty in the simulations instead of the
 174 accuracy of parameters used in the petrophysical relationships.



175
 176 **Figure 2.** A) The (vertically exaggerated for clarity) 2D transect mesh used by the ATS model. Green
 177 represents the peat layer and brown represents the mineral soil layer. Black stars correspond to the 6
 178 sensors collecting temperature and soil moisture content within the active layer. Red stars correspond
 179 to the 4 sensors collecting temperature and soil moisture content below the active layer. B) Ground
 180 temperature distribution simulated by the ATS model, corresponding to the time of maximum
 181 subsurface thaw. The active layer thickness corresponds to the linear white region (i.e., $0^\circ C$ region)
 182 dividing the thawed and frozen regions of the ground.



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Figure 3. Vertical transects of example model simulation results of liquid and ice saturation (rows) over winter and summer time periods (columns).

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187 2.2 Parameter estimation

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To test if the known soil properties can be recovered, we start with randomly selected initial parameter guesses as if the synthetic truth is unknown. We use a Latin Hypercube Sampling method to generate random initial guesses of porosity and thermal conductivities around the synthetic truth (McKay et al., 1979). Each sample set includes four parameters: porosity and thermal conductivity for peat and mineral soil layers. The rest of the hydrothermal properties are kept fixed. These parameters were chosen due to their strong controls on both hydrologic and thermal states (Atchley et al., 2015, Nicolsky et al., 2009).



195 The inverse approach involves the minimization of a cost function expressed as the sum-of-squared
196 differences between simulated values and synthetic measurements using the Levenberg-Marquardt
197 (LM) algorithm (K. Levenberg, 1944; D. W. Marquardt 1963) implemented in the PEST software
198 package (Doherty, 2001), which was used to handle all parameter estimation runs.

199 To estimate soil physical properties, we minimize the cost function (J) representing the sum-of-
200 squared differences between the calculated and synthetic T , s_l , and r in the following form:

$$201 \quad J(\phi, k) = w_T \sum (T_c - T_s)^2 + w_s \sum (s_{l_c} - s_{l_s})^2 + w_r \sum (r_c - r_s)^2, \quad (3)$$

202 where indices c and s correspond to calculated and synthetic states of the system, w_T , w_s , and
203 w_r are the corresponding weights for the temperature, saturation and resistance residuals
204 (differences between calculated and synthetic values).

205 The weights were chosen in order to scale the contribution of each type of residual so that
206 contributions to the cost function are evenly distributed across temperature, saturation, and
207 resistance residuals. For example, saturation residuals are on the order of a few tenths, while
208 resistance residuals can be tens of ohms. The weights were selected based on evaluating the
209 individual contributions to the cost function for each measurement type on an ensemble of
210 simulations spanning the parameter ranges. The electrical resistance residual weight (w_r) was set
211 to one. The temperature and saturation residual weights (w_T and w_s) were then modified so that
212 each measurement type component in the cost function had roughly equivalent magnitude over
213 most of the parameter space. This resulted in weights of $w_r=1$, $w_T=2.5 \times 10^3$, and $w_s=3.5 \times 10^5$.

214 If the cost function satisfies minimum criteria or the maximum allowed number of iterations, which
215 we chose to be equal to 25, is reached. The subsurface properties corresponding to the minimum
216 of the cost function, i.e., the best fit between simulated and synthetic values, are considered the
217 estimated parameter values as

$$218 \quad \{\phi, k\} = \underset{\substack{\phi_{min} \leq \phi \leq \phi_{max}, \\ k_{min} \leq k \leq k_{max}}}{\text{argmin}} J(\phi, k), \quad (4)$$

219 here $\{\phi, k\}$ are estimated porosities and thermal conductivities for peat and mineral soil.

220 Based on sensitivity analyses using simplified meteorological data, the cost function response
221 surface was smooth and convex over the parameter ranges of interest. Therefore, we chose the LM
222 approach because of its robust gradient-based optimization scheme that takes advantage of smooth
223 convex response surfaces to quickly converge to minima.



224 To build an understanding of the inverse framework, we start with a simple setup and then
 225 gradually add more complexity. First, we use simplified meteorological data where we assume
 226 that air temperatures change according to a sinusoidal function and all other terms are constants.
 227 Initially we started with 3 observational points within the peat layer (refer to Figure 2A) and 1
 228 ERT profile. Then we increase the number of ERT profiles up to 8 by adding profiles once per
 229 month from January till August. Each ERT profile calculated by BERT uses the set of daily
 230 averaged T and s_l simulated by ATS and petrophysical relations (eqn. 2) which are varying over
 231 time. Then we increase the number of observation points to 6 and add noise to the simulated data.
 232 Introduction of the noise allows us to evaluate the effect of measurement uncertainties that will be
 233 present in the actual application of the PE method. We added different levels of Gaussian noise to
 234 the synthetic measurements of T , s_l , and r in the following way: 1% to T , 5% to s_l , and 10% to r .
 235 These levels of noise for the different types of measurements are based on published literature and
 236 our own experience (Wang et al., 2018; Dafflon et al., 2017). After that we substitute simplified
 237 meteorological data with actual data from the BEO site to evaluate our PE method under realistic
 238 ground surface boundary conditions. In this case we evaluate how much and what kind of data do
 239 we need to robustly recover subsurface porosities and thermal conductivities. To do this we test
 240 the inclusion of individual types of measurements in the cost function (equation 3) as well as all
 241 possible combinations of measurement types. We used different soil property ranges for the
 242 simplified and actual meteorological data PE runs which are summarized in Table 1. This was
 243 done to test the consistency and effectiveness of the PE method. In addition, we compared the
 244 difference between estimated parameters for 8 ERT profiles collected once a month for 8 months
 245 versus once a day for 8 days. Notation and description of each run for simplified and actual
 246 meteorological data is summarized in Table 2.

247 **Table 1: Allowed range for the estimated subsurface properties.**

Properties	Simplified meteorological data		Actual meteorological data	
	peat	mineral	peat	Mineral
Porosity [$m^3 \cdot m^{-3}$]	0.8±1.9	0.6+0.25	0.6±1.9	0.4+0.25
Thermal conductivity, [$W m^{-1}K^{-1}$]	0.225±0.2	2.0±0.5	0.15±0.1	1.6±0.5

248

249 **Table 2: Description of all PE cases used in this study.**



Case number	Simplified meteorological data (S)*	Actual meteorological data
1	(S)3T3s _l 1r	6T
2	(S)3T3s _l 8r	10T
3	(S)6T6s _l 1r	6s _l
4	(S)6T6s _l 8r	1r
5	(S)6T6s _l 1r+n	6T1r
6	(S)6T6s _l 8r+n	6s _l 1r
7		6T6s _l
8		3T3s _l 1r
9		3T3s _l 8r
10		6T6s _l 8r
11		6T6s _l 8r(s)**
12		10T10s _l 1r
13		10T10s _l 8r

250 The numbers before T and s_l correspond to the number of measurement points used. Number before r
 251 corresponds to the number of resistance profiles used.

252 n stands for noise added to the synthetic measurements.

253 *(S) corresponds to runs driven by simplified meteorological data, no (S) corresponds to runs driven with
 254 actual meteorological data

255 **All resistance profiles are taken once per month, except the case with (s) corresponding to sequential daily
 256 profiles.

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258 3. Results

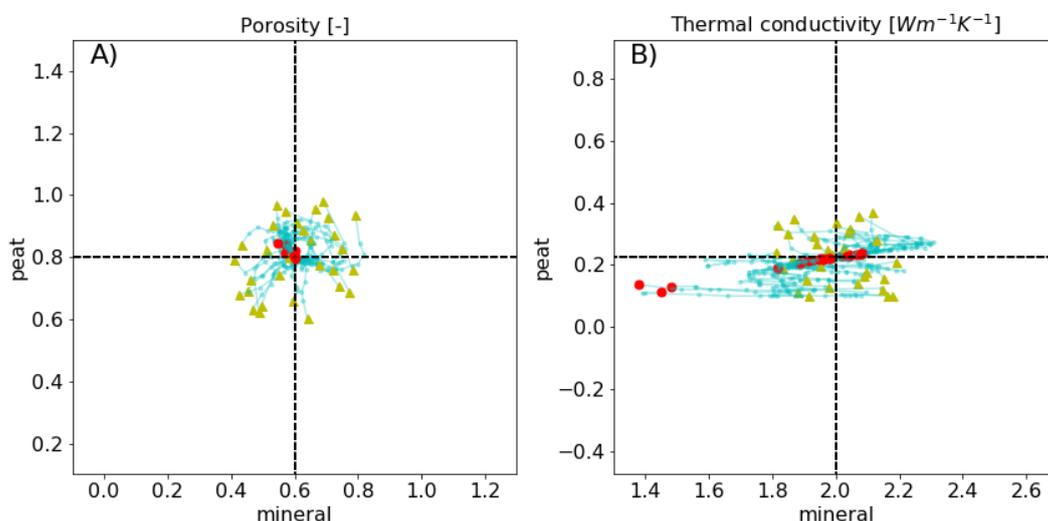
259

260 3.1 Simplified meteorological data

261 To evaluate the PE method performance driven by simplified meteorological data, we ran PE
 262 experiments using 30 different random combinations of porosity and thermal conductivity values
 263 as the initial starting point. It is important to note that one of the main points of this study is to
 264 demonstrate that one or two LM runs might lead to false assumptions about recovered parameters.
 265 Multiple runs starting from different initial guess values are necessary to ensure the robust
 266 recovery of the subsurface conditions. If most of the LM runs converge to the same set of
 267 parameters and have low cost function values, then that set most likely corresponds to the actual
 268 subsurface properties. In Figure 4, the yellow triangles represent initial guesses (i.e. inversion



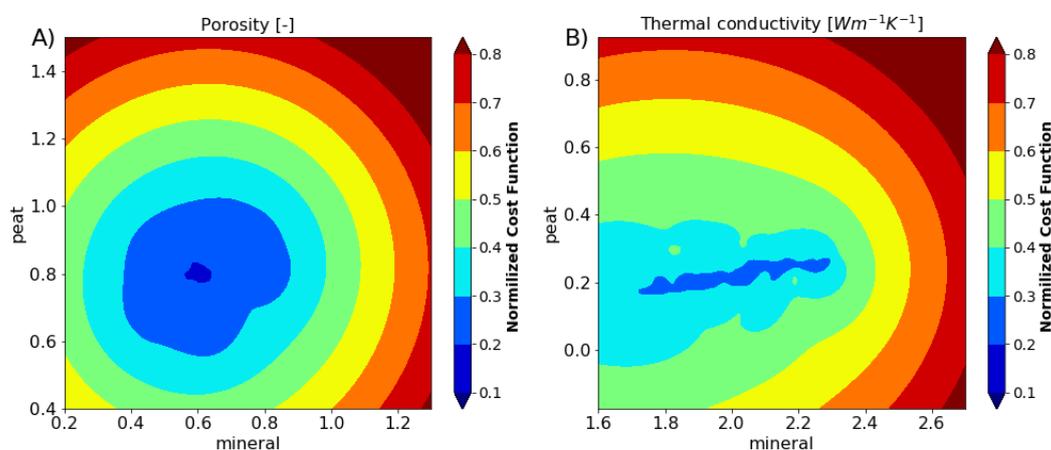
269 parameter combination starting points). In these plots, the synthetic truth is indicated by the
270 intersection of the two dotted lines. Bright turquoise lines connecting yellow triangles with red
271 dots represent the path that the LM algorithm has taken from the initial guess to the estimated
272 parameter combination represented by the red dot. The dots connecting turquoise lines indicate the
273 location at each LM iteration. Figure 4 indicates that the method is able to recover porosities more
274 robustly than thermal conductivities. According to the liquid saturation plot on Figure 3, liquid
275 saturation of the mineral layer is quite dynamic and more saturated in comparison to the peat layer.
276 Nevertheless, thermal conductivity of the mineral layer corresponds to the highest uncertainty.
277 Three out of thirty red dots corresponding to thermal conductivity of mineral soil end up close to
278 $1.4 \text{ W m}^{-1}\text{K}^{-1}$ (the true value is $2 \text{ W m}^{-1}\text{K}^{-1}$), suggesting those values do not correspond to the
279 ‘truth’, since most of the estimated values (27 cases) are concentrated around the intersection of
280 the dotted lines. In this case the response surface for the corresponding cost function (eqn. 3) lies
281 in a flat, low-gradient region. This effect can be seen in Figure 5, the cost function corresponding
282 to the estimated porosities (Figure 5A) has only one minimum, where the cost function
283 corresponding to thermal conductivities (Figure 5B) has an elongated flat minima region indicating
284 non-uniqueness of the estimated parameters. This case corresponds to the 6 near-surface
285 observation points (Figure 2A) with short vertical distance between the points. The close proximity
286 of the observation locations might be limiting variability in the calibration targets leading to
287 difficulty in estimating the k_m parameter.



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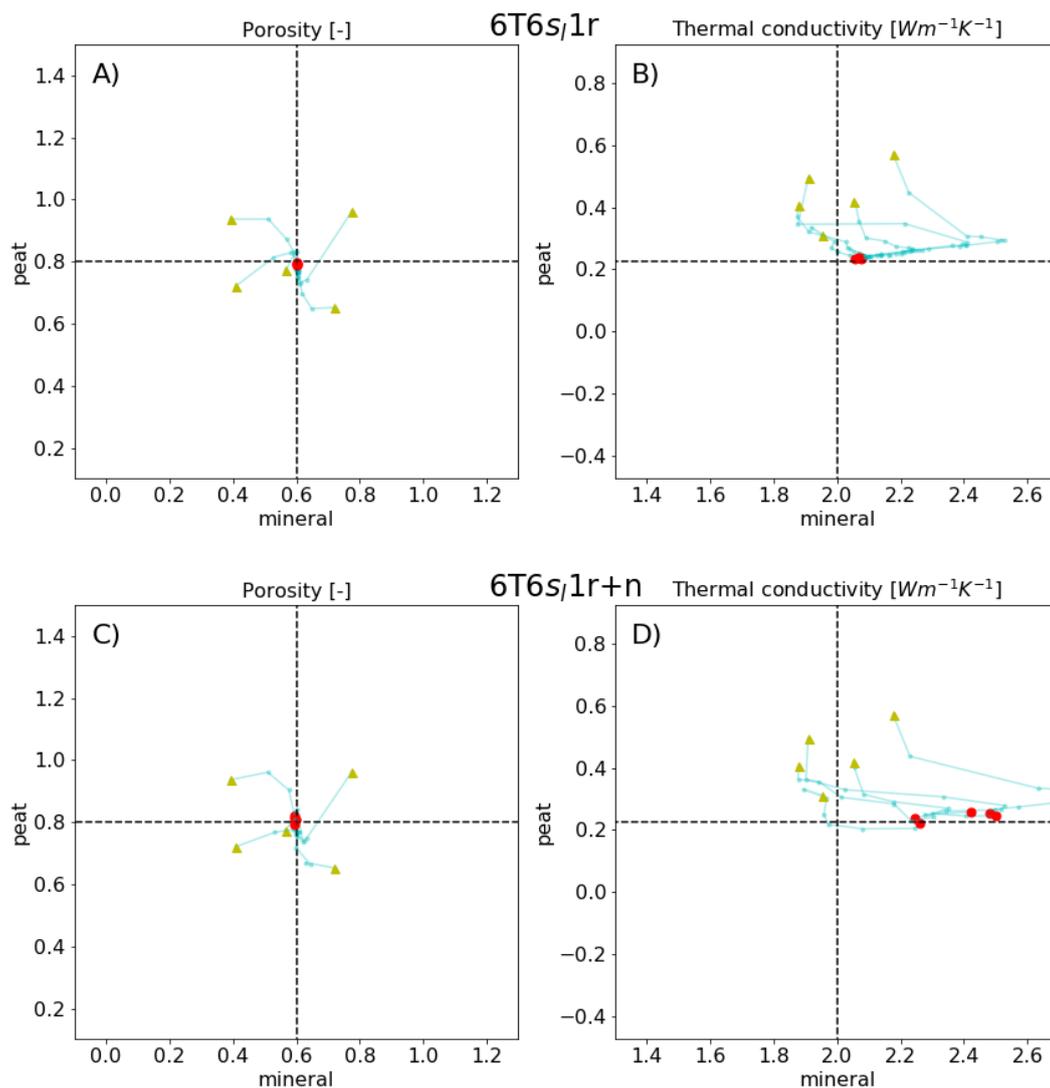
289 **Figure 4.** Estimated values of a sample of 30 initial guesses to their “true” values shown as a cross-
290 section of two dotted lines for A) porosities and B) thermal conductivities for peat mineral soil layers. Blue
291 lines correspond to different paths that have been taken by the LM algorithm. The red dots correspond to
292 the estimated parameter values. Note that subfigures (A) and (B) are each showing 2D projections of the
293 4D parameter space of the inversion.

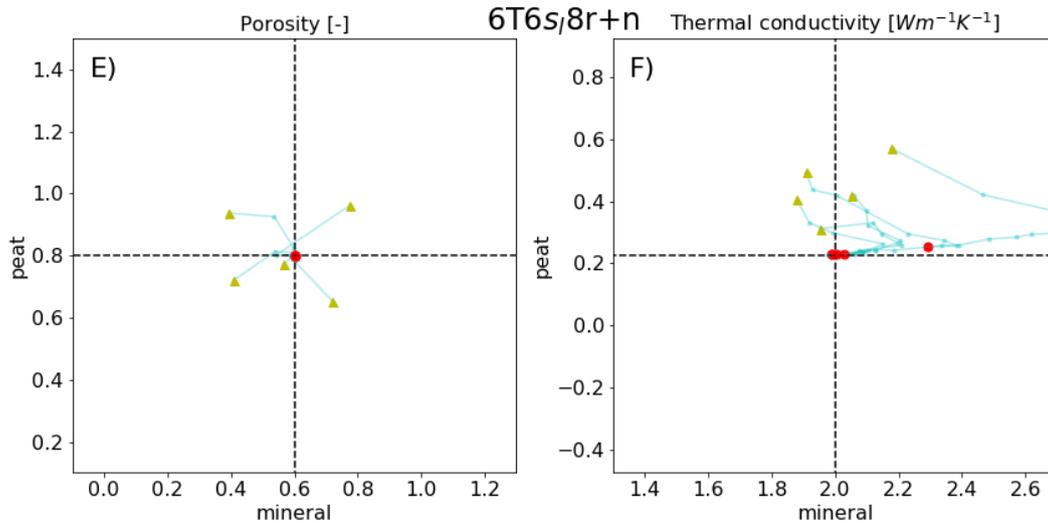


294 **Figure 5.** Cost function corresponding to A) porosities and B) thermal conductivities for peat and mineral
295 soil layers. Here, the colorbar is a normalized cost function. Note that subfigures (A) and (B) are showing
296 2D projections of a 4D parameter space that the inverse approach was applied to.
297

298

299 Figure 6 illustrates estimated parameters for all cases corresponding to simplified meteorological
300 data from Table 2. Figure 6AB shows good convergence of the (S)6T6S₁1r case for porosities and
301 worse convergence for thermal conductivities with an averaged error of $0.1Wm^{-1}K^{-1}$. Adding
302 noise to the (S)6T6S₁1r+n case slightly worsens the estimated porosity values and significantly
303 worsens mineral soil thermal conductivity with RMSE raising from 10% to more than 50% (Figure
304 6CD). Figure 6EF shows that increasing the number of the monthly ERT profiles from 1 to 8
305 improved soil property estimates, allowing four out of five PE runs to converge closer to the
306 synthetic truth. If we do not consider the one outlier on the conductivity plot (Figure 6F) for case
307 (S)6T6S₁8r+n then uncertainty is smaller than for the (S)6T6S₁1r case (without noise), suggesting
308 that despite introduction of the 10% noise to the ERT data increasing the number of the monthly
309 ERT profiles improves the overall PE.





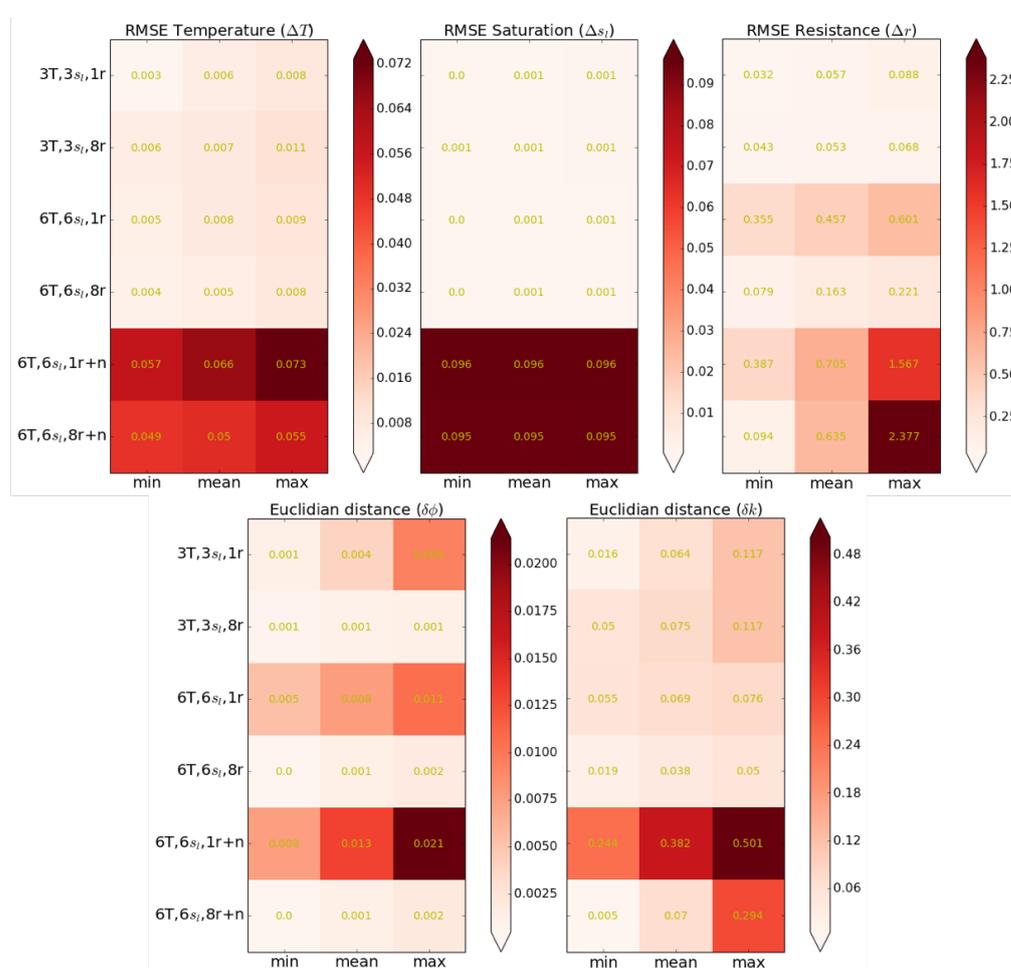
310 **Figure 6.** Estimated values of a sample of 5 initial guesses to their “true” values shown as a cross-section
 311 of two dotted lines for the bulk porosities and bulk thermal conductivities for peat mineral soil layers. Blue
 312 lines correspond to different paths that have been taken by the LM algorithm. The red dots correspond to
 313 the estimated values. A-B) 6 observation points and 1 ERT resistance profile $(S)6T6s_l I r$; C-D) 6
 314 observation points and 1 ERT resistance profile with added noise $(S)6T6s_l I r+n$; E-F) 6 observation
 315 points and 8 ERT resistance profile with added noise $(S)6T6s_l 8r+n$. Note that the plots are each 2D
 316 projections of the 4D parameter space of the inversion.

317

318 In Figure 7, we summarize results from the five PE runs for the first six cases corresponding to
 319 simplified meteorological data listed in Table 2. The first row of tables corresponds to the final
 320 root-mean-squared error (RMSE) values for each measurement type (ΔT , Δs_l , and Δr). The second
 321 row of tables corresponds to the Euclidian distances between the synthetic truth and estimated
 322 parameter values of $\delta\phi$ and δk . As it was shown above, the method is able to accurately estimate
 323 both peat and mineral soil porosities and peat layer thermal conductivity (k_p), but cannot always
 324 accurately estimate the thermal conductivity of the mineral soil (k_m). That is why the matrix table
 325 with estimated thermal conductivities on Figure 7 shows the highest discrepancy (bottom row, last
 326 table). However, one can see from the ϕ and k matrix tables that increasing the number of monthly
 327 ERT profiles improves the estimates of ϕ and k . This suggests that by increasing the number of
 328 monthly ERT profiles, we are improving the convexity of the cost function (eqn.3). Increasing the
 329 number of T and s_l observational points from 3 to 6 has a less significant effect on estimated



330 values of ϕ and k . This could be due to the fact that all 6 observational points lie within the active
 331 layer zone. Suggesting that adding observations below the active layer might have more significant
 332 effect on the estimated properties. Therefore, we added extra observational points (red stars in
 333 Figure 2A), to test this assumption in the experiment with actual meteorological data.
 334



335
 336 **Figure 7.** Five matrix tables presenting fitness metrics between synthetic model values and values
 337 obtained by the parameter estimation method using simplified meteorological data. First row corresponds
 338 to the root mean squared errors for temperatures, liquid water saturations, and resistances. Second row
 339 includes tables corresponding to Euclidian distances between synthetic (“true”) and estimated parameter
 340 values.
 341

342 3.2 Meteorological data from Utqiagvik (Barrow) site 2015



343 After testing the PE method for the simplified meteorological data, we applied measured
344 meteorological data from the BEO site for year 2015. To better understand the importance of each
345 measurement type and their combinations within the developed PE framework we tested all of the
346 scenarios corresponding to the ‘actual meteorological data’ column from Table 2. The results of
347 these runs are summarized in the colored matrix tables in Figure 8. Since there are twice the
348 number of actual meteorological cases than the simplified meteorological cases, it is hard to
349 analyze all matrix tables at once. To combine the data from all five matrices we normalized the
350 mean values in the middle column in each table by their maximum value as $\tilde{\Delta} = \frac{\Delta}{\Delta_{max}}$ and $\tilde{\delta} =$
351 $\frac{\delta}{\delta_{max}}$. This normalized the magnitudes of different measurement and soil property types. Then we
352 calculated the RMSE of the normalized mean values for combined measurement and soil property
353 types, $\Delta(\tilde{\Delta T}, \tilde{\Delta s}_1, \tilde{\Delta r})$ and $\Delta(\tilde{\delta \phi}, \tilde{\delta k})$, respectively. Based on these normalized and combined
354 RMSE values, we used k-mean clustering analysis to identify groupings of data collection
355 strategies that result in similarly performing inversions. The analysis identified four clusters of
356 data collection strategies resulting in similarly performing inversions shown in Figure 9. Class I
357 and II indicate all the cases that provide good accuracy for the estimated properties. Class I
358 indicates the best cases that provide an accurate parameter estimation as well as accurate matches
359 with the synthetic “true” measurements. Class II includes the cases that have accurate parameter
360 estimates and less accurate matches with the measurements. Class III indicates all cases that have
361 less accurate parameter estimates but accurate matches with the measurements. Finally, Class IV
362 includes the cases that showed the worst performance in terms of parameter estimates and the
363 worst matches with the measurements. We summarized the results from Figure 9 in Table 3.
364 Cases in Class I (see Table 3) suggest that measurement locations below the active layer lead to
365 better PE, meaning that by increasing the number of measurement locations leads to more accurate
366 parameter estimation. In contrast, the last element of the first class is a case with one ERT profile
367 (1r), suggesting that one ERT profile could be enough for effective parameter estimation. This is
368 due to the design of this numerical experiment, i.e. due to the fact that we are using a synthetic
369 “truth” produced by the same model used in the inversion, which improves the convexity of the
370 cost function and leads to a well constrained unique minimum. However, in reality, collection of
371 the additional information, such as organic layer thickness and temperature data, are extremely
372 important and are required for model calibration (Jafarov et al., 2012; Atchley et al., 2015). In



373 addition, real ERT surveys can be perturbed by noise and their interpretation may require site-
 374 specific petrophysical relationships as opposed to the general petrophysical relationships used in
 375 this study. Therefore, we do not suggest to collect only one ERT measurement without any
 376 additional data.

377 Class II indicates that increasing the number of monthly ERT profiles is important for more
 378 accurate PE. However, increasing the number of ERT profiles leads to a less accurate match with
 379 measurements. These results are consistent with the previous results for simplified data and added
 380 noise (Figure 6).

381 Class III includes 6 cases suggesting that if we have only soil moisture data available for PE, then
 382 we should expect less accurate soil property estimates. The last element in this class suggests that
 383 collecting daily resistance profiles improves the resistance match (Figure 8, resistivity table) but
 384 does not improve soil property estimates, where monthly ERT profiles improve thermal
 385 conductivity convergence.

386 Class IV once again clearly indicates that measurements obtained below the active layer provide
 387 more accurate parameter estimates, however, they do not improve matches to measurements. This
 388 is mainly due to significant mismatch with the ERT data, which can be seen on the RMSE
 389 resistance table (Δr) in Figure 8. In reality, the depth of the mineral soil can be deeper than 20 cm,
 390 not having sensors lower than 20 cm limits the amount of data that can help to improve the
 391 convexity of the cost function in our case.

392 **Table 3:** K-mean analysis of the accuracy for each 13 cases.

Class I	Class II	Class III	Class IV
$10T10s_l lr$	$6T6s_l 8r$	$6s_l$	$10T$
$10T10s_l 8r$	$3T3s_l 8r$	$6s_l lr$	$6T$
lr		$6T lr$	
		$3T3s_l lr$	
		$6T6s_l$	
		$6T6s_l 8r(s)$	

393

394 From Figure 9 and Table 3 we know that the $6T$ case has the worst performance in terms of
 395 matching $\{\phi, k\}$. Similar to the experiments with simplified meteorological data, the main
 396 difficulty for experiments with actual meteorological data is matching thermal conductivity. The



397 last matrix table ($\sigma(k)$) on Figure 9 shows that $6T6s_l\delta r(s)$ has the highest maximum and mean
398 mismatch in thermal conductivity estimates. However, since ϕ estimates are a better match with
399 their corresponding “true” values, the case $6T6s_l\delta r(s)$ falls into class III in Figure 9, as opposed
400 to case $6T$, which falls into class IV. The highest mismatch in thermal conductivity values for the
401 $6T6s_l\delta r(s)$ case suggests that collecting daily resistance profiles improves the resistance match
402 (Figure 8, resistivity table) but does not improve estimated parameters, where monthly ERT
403 profiles improve thermal conductivity estimation.

404 To illustrate this, we plot values of estimated thermal conductivities and the corresponding cost
405 functions for cases $10T10s_l\delta r$ and $6T6s_l\delta r(s)$ on Figure 10. The PE method was able to match 4
406 out of 5 points perfectly and missed the k_p for the $10T10s_l\delta r$ case. The corresponding cost
407 function is almost perfectly convex with only one minimum. In contrast to this, the $6T6s_l\delta r(s)$
408 case completely missed 2 points by converging on values outside the boundaries, and 3 other points
409 do not converge to the desired cross section as well. The corresponding cost functions does not
410 have a well-defined global minimum.

411

412 **4. Discussion**

413

414 The existence of multiple minima is common in inverse modeling and leads to false convergence
415 of the LM algorithm and physically non-realistic subsurface parameters (Nicolosky et al., 2007).
416 This is one of the main reasons of using multiple initial guesses. We suggest to run at least ten
417 different initial guesses. If most of those runs converge to a similar set of values with the lowest
418 cost function value, then that set of values is most likely the global minimum.

419 There will always be cases like $6T6s_l\delta r(s)$, where all runs converge to different values of k_m ,
420 indicating that using certain combinations of datasets does not allow the inverse approach to
421 properly recover k_m . It is likely that $6T6s_l\delta r(s)$ does not capture much variability in soil
422 temperatures and soil moisture and therefore ERT profiles do not have much variability as well.
423 Once the cost function converges for one of the ERT profiles, it immediately converges on the
424 other daily profiles. In fact, although $6T6s_l\delta r(s)$ has a good accuracy with observations (see the
425 “RMSE Resistance” table in Figure 8), it is unable to recover the value of k_m . Here, a
426 regularization technique may improve the corresponding data accuracy. The regularization



427 techniques have been widely used in solving ill-posed inverse problems (Vogel, 2002). Its overall
428 idea is to constrain the objective function by imposing additional priors on the estimated model
429 parameters. The PEST package allows us to add a regularization term to the cost function (eqn.
430 4). In particular, the PEST package provides several categories of regularization techniques
431 including Tikhonov regularization, subspace-type of regularization, and hybrid regularization.
432 Tikhonov regularization, being the most commonly used regularization technique in inverse
433 problems, imposes a L2 norm constraint on the estimated model parameters (Vogel, 2002). The
434 resulting cost function tends to be smoother over the parameter space. The subspace regularization
435 technique is developed based on truncated singular value decomposition. It promotes the
436 numerical stability of the iteration by discarding the eigenvectors associated with small singular
437 values so that the solution space can be spanned by the dominant eigenvectors. The hybrid
438 regularization technique is a combination of Tikhonov regularization and subspace regularization
439 techniques. The numerical results presented in this manuscript demonstrates that our problems
440 may not be severely ill-posed. Hence, reasonable results can be obtained with enough data
441 coverage. Having regularization techniques incorporated into our current method may help to
442 constrain the estimated parameters from significant divergence as in Figure 10C. However,
443 exploration of the regularization options in PEST requires in depth experimentation beyond the
444 scope of the current study.

445 We have shown that even in the ideal situation where we either generate observational data or use
446 simplified meteorological data, we cannot always fit modeling results to observations. In reality,
447 noise (e.g. sensor's measuring resolution) contaminates the observational data. To investigate the
448 impact of measurement noise, we introduced multiple levels of noise to the simplified
449 meteorological data. The PE showed that dealing with noisy data is challenging, even for a simple
450 cases (Figure 6). However, our analysis showed that adding more data into the cost function (in
451 particular resistivity data) can improve the overall PE accuracy.

452 The distance between sensors could be another reason that might lead to the uncertainty in PE. As
453 it was pointed out by Nicolsky et al., (2009), it is important to make sure that a vertical difference
454 between the adjacent measurements do not introduce additional noise that can confuse the
455 minimization algorithm. If sensors are really close to each other, then measurements might be the
456 same or within the noise variability. In our setup the vertical distance between the first 6 sensors
457 is about 10cm. This could lead to small temperature variability between sensors. Indeed, providing



458 greater vertical distance between observational points improved the PE accuracy (see cases with
459 10 observational points).

460 Combining hydrothermal observations from multiple depths with monthly ERT measurements
461 resulted in improving the shape of the cost function leading to better defined minima (Figure 10).
462 Increasing the number of the monthly ERT profiles improved the accuracy of the estimated data.
463 In addition, we showed that having observation points below the ALT combined with ERT profiles
464 shows the best accuracies both in the terms of estimating parameters and matching observations.

465

466 **5. Conclusion**

467

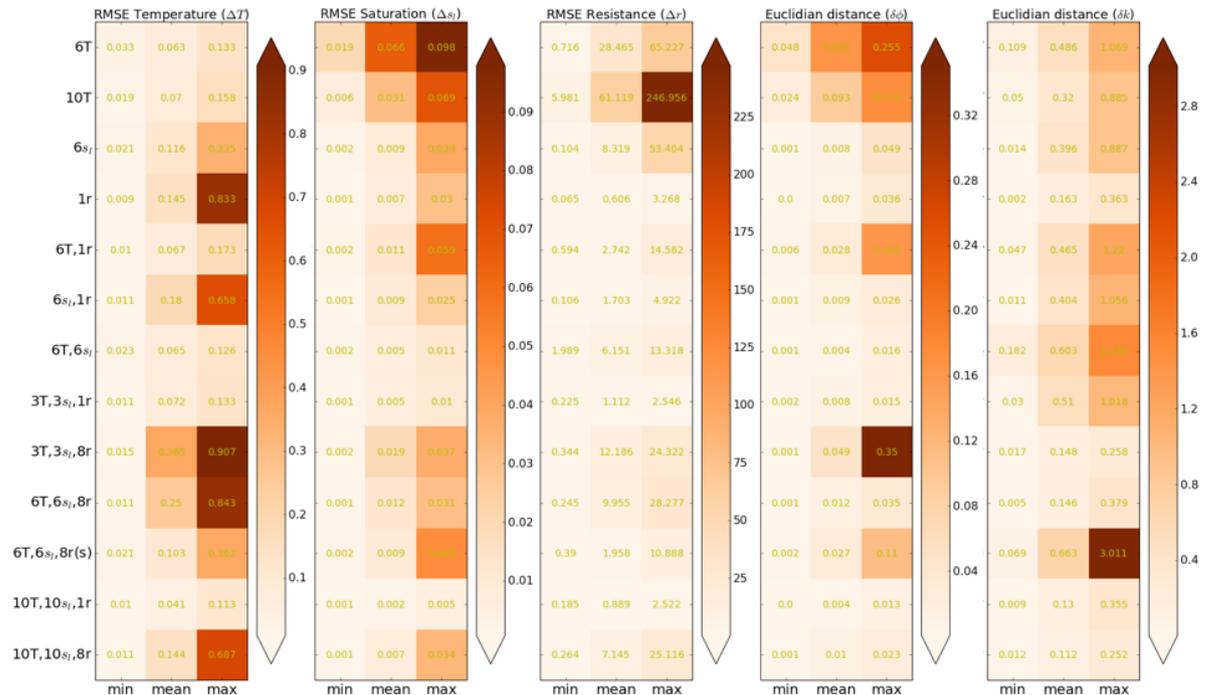
468 The overarching goal of this study was to validate a newly developed PE framework using a
469 synthetic setup and 2D coupled thermal-hydro-geophysical model based on the polygonal tundra
470 at the BEO study site. The results of this study show that estimating subsurface properties even for
471 a synthetic setup can be quite complicated. Nevertheless, the PE method evaluated here shows that
472 there are cases when the method is able to robustly recover synthetic properties. The robustness of
473 the method depends on the frequency and diversity of the collected data. For example, we found
474 that adding monthly ERT surveys into the cost function significantly improves the accuracy of the
475 estimated properties. It is important to note that to improve the overall robustness of the PE, it is
476 better to collect such data from multiple depths within and below the active layer. Furthermore,
477 we conclude that different data types query the system in different ways; we find that the most
478 robust predictions result from inversions that include multiple data types.

479 As it was shown in this study, different measurement types as well as a combination of multiple
480 measurements might lead to the different shapes of the cost function with multiple minima and/or
481 ill-defined global minimum (flat spots in the response surface). To improve the overall PE
482 performance we suggest the following: 1) restricting of the parameter range to better constrain the
483 local minimum; 2) introducing different types of data (T, s_l, r) into the cost function to improve PE
484 accuracy. If most of the runs from the sample converge to the same parameter values and the cost
485 function is lower at this location, then those values most likely correspond to the actual soil
486 properties. The ability to refine the cost function with more data (monthly ERT and timeseries
487 from multiple depths) has to be further explored with actual data.



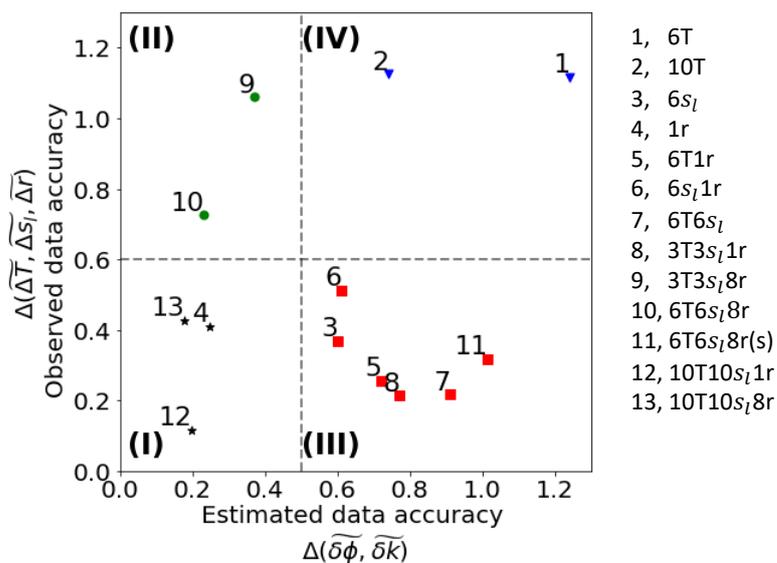
488 Implication of the PE method to the actual measured data might require adjustment of the initial
 489 conditions of the model (saturation and temperature). Incorporating the initial condition data into
 490 the PE framework might lead to a better match with actual subsurface observations. This work
 491 demonstrates the feasibility of the developed PE framework. However, further evaluation of
 492 regularization methods and recovery of the soil properties using measured subsurface data from
 493 the BEO site is needed and are beyond the scope of the current paper.

494



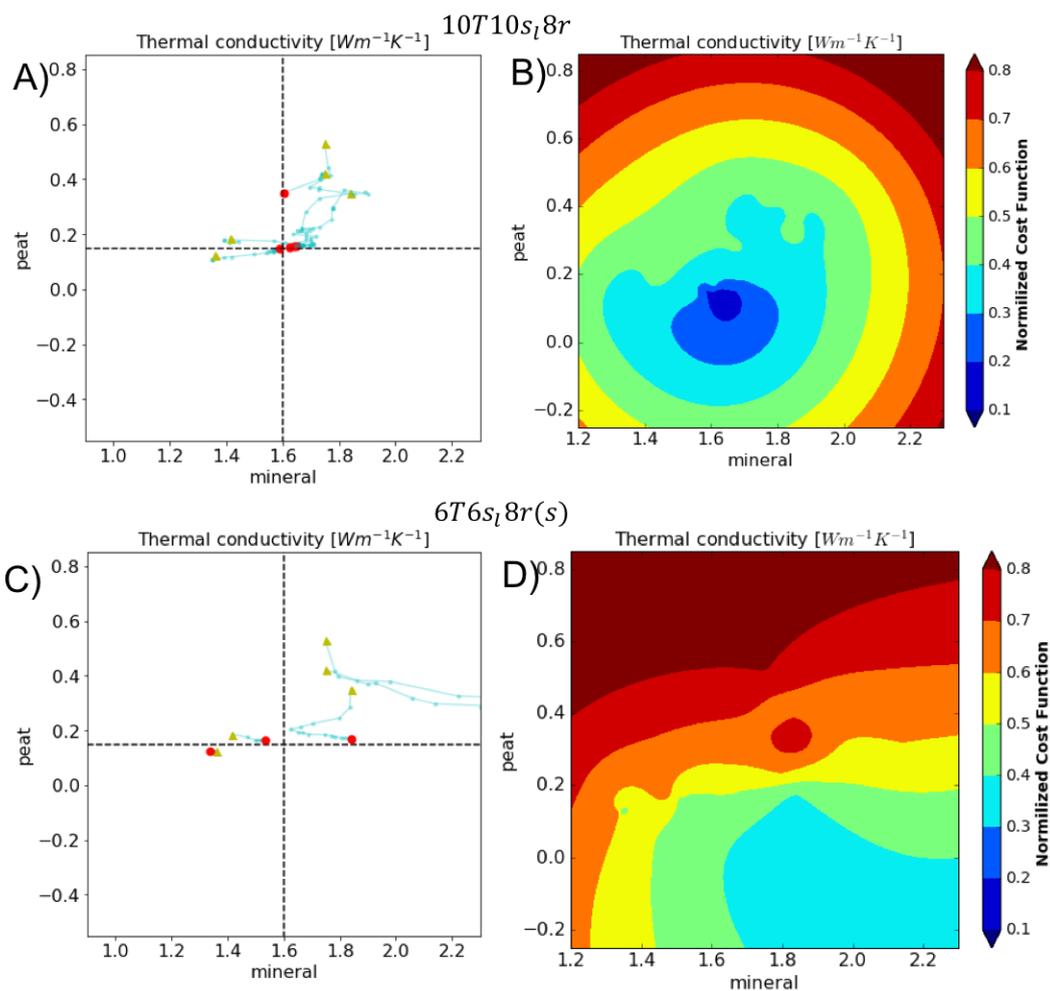
495

496 **Figure 8.** Five matrix tables represent fitness metric between synthetic model values and values obtained
 497 by the parameters estimation method using meteorological data from year 2015 from BEO site in Alaska.
 498 First three tables correspond to the root mean squared values for temperatures, liquid water saturations,
 499 and resistances, the last two tables correspond to Euclidian distances between synthetic and estimated
 500 conductivities and porosities, correspondingly.



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Figure 9. A k-mean analysis applied to the RMSE of the normalized means of estimated soil properties and the corresponding fit between calculated and observed values. Each color and marker represent a certain class as result of the k-mean cluster analysis.



506
 507 **Figure 10.** A) and C) parameter search trajectories for 5 inversions where the “true” values are shown as
 508 a cross-section of two dotted lines for the bulk porosities and bulk thermal conductivities for peat mineral
 509 soil layers. Blue lines correspond to different paths that have been taken by the LM algorithm. The red
 510 dots correspond to the estimated parameter values. First row corresponds to 10 measurement locations
 511 and 8 ERT resistance monthly profiles ($10T10s_l8r$), and the second row corresponds to 6 measurement
 512 locations and 8 ERT resistance daily profiles ($6T6s_l8r(s)$). B) and D) the colormap plots on the right
 513 represent the cost function values associated with the corresponding thermal conductivities.

514

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519

520 **6. References**

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